

### ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM

#### Laura Karen Acosta Capilla

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# ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM

Ph.D Thesis

Supervised by:

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Departament D'Enginyeria Electrònica Elèctrica i Automàtica Nanoelectronic and Photonic Systems (NePhoS)



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I, Lluís Francesc Marsal Garví state that the present study, entitled "ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM", presented by Laura Karen Acosta Capilla for the award of the degree of Doctor, has been carried out under my supervision at the Department of Electronic, Electric and Automatic Control Engineering of this university and that it satisfies all requirements to be eligible for the International Doctorate Award.

Tarragona, June 18<sup>th</sup>, 2021 Doctoral Thesis Supervisor

Lluís Francesc Marsal Garví

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#### **List of Contributions**

#### **Journal Articles**

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- Laura K Acosta, Francesc Bertó-Roselló, Elisabet Xifre-Perez, Abel Santos, Josep Ferré-Borrull and Lluis F. Marsal. "Stacked nanoporous anodic alumina gradient-index filters with tunable multi-spectral photonic stopbands as sensing platforms". ACS Applied Material and interfaces 2019, 11, 3360-3371.
- Laura Pol, Chris Eckstein, Laura K. Acosta, Elisabet Xifré-Pérez, Josep Ferré-Borrull and Lluis F. Marsal. "Real-Time Monitoring of Biotinylated Molecules Detection Dynamics in Nanoporous Anodic Alumina for Bio-Sensing". Nanomaterials, 2019, 9 (3), 478.
- Laura Pol, Laura K. Acosta, Josep Ferré-Borrull and Lluis F. Marsal. "Aptamer-Based Nanoporous Anodic Alumina Interferometric Biosensor for Real-Time Thrombin Detection". Sensors. 2019. 19 (20), 4553.
- Laura K Acosta, Francesc Bertó-Roselló, Elisabet Xifre-Perez, Cheryl Suwen Law, Abel Santos, Josep Ferré-Borrull and Lluis F. Marsal. "Tunable Nanoporous Anodic Alumina Photonic Crystals by Gaussian Pulse Anodization". ACS Applied Materials & Interfaces. 2020, 12 (17). 19778-19787

- Lluis F. Marsal, Laura K. Acosta, Josep Ferrè-Borrull. "Recent Advances in Structural Engineering of Nanoporous Anodic Alumina and Applications". ECS Transactions. 2020. 98 (2). 3-11
- 7. Siew Yee Lim, Cheryl Suwen Law, Lin Jiang, Laura K Acosta, Akash Bachhuka, Lluís F Marsal, Andrew D Abell, Abel Santos. "Enhancing Forbidden Light Propagation in Nanoporous Anodic Alumina Gradient-Index Filters by Alcohol Additives". *ACS Applied Nanomaterials*. 2020. 3 (12). 12115-12129
- 8. Lina Liu, Siew Yee Lim, Cheryl Suwen Law, Laura K Acosta, Bo Jin, Andrew D. Abell, Lluis F Marsal, Gang Ni, Abel Santos. "Optical engineering of nanoporous photonic crystals by Gaussian-Like pulse anodization". *Microporous and Mesoporous Materials*. **2021.** 312. 110770
- Pankaj Kapruwan, Laura K. Acosta, Josep Ferre-Borrull, Lluis F. Marsal. "Optical platform to analyze a model drug loading and releasing profile based on Nanoporous Anodic Alumina Gradient Index Filters". Nanomaterials 2021, 11, 730.
- Laura K Acosta, Cheryl Suwen Law, Siew Yee Lim, Andrew Abell, Lluis F. Marsal and Abel Santos. "Role of Spectral Resonance Features and Surface Chemistry in Optical Sensitivity of Light-Confining Nanoporous Photonic Crystals". ACS Applied Materials and Interfaces. 2021, 13,12, 14394–14406.
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- Nanospain 2017. Surface modification of Nanoporous Alumina towards bio-sensing applications in optical nano-fluidic system. L. Pol, <u>L. K. Acosta</u>, J. Ferré-Borrull, E. Xifre-Pérez, L. F. Marsal. <u>Poster</u>
- NanoBio&Med 2017. Stacked periodic nanoporous anodic alumina structures for sensing applications. <u>Laura K. Acosta</u>
   Capilla, Elisabet Xifré-Perez, Josep Ferré-Borrull, Lluis F. Marsal. <u>Poster</u>
- NanoBio&Med 2017. Interferometric real time monitoring Streptavidin bioconjugation in Nanoporous Anodic Alumina. L. Pol, L. K. Acosta, J. Ferré-Borrull, L. F. Marsal. <u>Poster</u>
- Porous Semiconductures Science and Technology conference (PSST) 2018. Nanostructured sensing platform based on multiple periodic structures of nanoporous anodic alumina. <u>Laura K.</u> <u>Acosta</u> Capilla, Elisabet Xifré-Perez, Josep Ferré-Borrull, Lluis F. Marsal. <u>Oral presentation</u>.
- 6. Porous Semiconductures Science and Technology conference (PSST) 2018. Numerical Modelling and Characterization of Nanoporous Anodic Alumina Rugate Filters. Francesc Bertó-Roselló, <u>Laura K. Acosta Capilla</u>, Elisabet Xifré-Perez, Josep Ferré-Borrull, Lluis F. Marsal. <u>Poster</u>

- 7. Porous Semiconductures Science and Technology conference (PSST) 2018. Influence of incubation time on the surface modification of nanoporous anodic alumina studied by fluid imbibition-coupled laser interferometry. C. Eckstein, I. Pol-Aira, <u>L.</u> <u>K. Acosta-Capilla</u>, E. Xifré-Pérez, J. FerréBorrull. *Oral Presentation*
- 8. Porous Semiconductures Science and Technology conference (PSST) 2018. Engineering and analysis of graded-index photonic nanostructures based on mesoporous anodic alumina. E. Xifré-Pérez, L. K. acosta, J. Ferre-Borrull, and L. F. Marsal. Poster
- Porous Semiconductures Science and Technology conference (PSST) 2018. Interferometric real-time monitoring of streptavidinbiotin conjugation in nanoporous anodic alumina. L. Pol, L. K. Acosta, J. Ferré-Borrull, E. Xifre-Pérez, L. F. Marsal. <u>Poster</u>
- 10. Reunion Nacional de óptica (RNO) 2018. Nanoporous anodic alumina rugate filters for optical biosensing. <u>Laura K. Acosta Capilla</u>, Francesc Bertó-Roselló, Elisabet Xifré-Perez, Josep Ferré-Borrull, Lluis F. Marsal. <u>Oral Presentation</u>
- 11. **Conferencia Española de nanofotónica (CEN) 2018**. Structural engineering of one-dimensional nanoporous anodic alumina photonic crystals. **Laura K. Acosta** Capilla, Elisabet Xifré-Perez, Josep Ferré-Borrull, Lluis F. Marsal. *Oral presentation*
- 12. Conferencia Española de nanofotónica (CEN) 2018. Study of Nanoporous Anodic Alumina Gradient-Index Structures by Numerical Modelling. Francesc Bertó-Roselló, <u>Laura K. Acosta</u> <u>Capilla</u>, Elisabet Xifré-Perez, Josep Ferré-Borrull, Lluis F. Marsal. <u>Oral Presentation</u>

- Conferencia Española de nanofotónica (CEN) 2018. Optical Characterization of the Attachment of Biotinylated Proteins in Nanoporous Anodic Alumina by means of RIfS. L. Pol, <u>L.K. Acosta</u>, J. Ferré-Borrull, E. Xifre-Pérez, L.F. Marsal. *Poster*
- Conferencia Española de nanofotónica (CEN) 2018. Study of physical and photonic properties of anodized alumina nanotubes.
   J.T. Domagalski, E. Xifre-Perez, <u>L. K. Acosta</u> and L. F. Marsal. <u>Poster</u>
- NanoSpain 2019. Stacked and Overlapped Photonic Structures in Nanoporous Anodic Alumina. Laura. K Acosta, Elisabet Xifre-Perez, Josep Ferré-Borrull, and Lluis F. Marsal. Oral presentation
- 16. NanoBio&Med 2019 Complex Nanoporous Anodic Alumina Photonic Structures for Sensing: Design, Fabrication and Application. Laura. K Acosta, Elisabet Xifre-Perez, Josep Ferré-Borrull, and Lluis F. Marsal. <u>Oral presentation</u>
- CDE 2021. Progress in Engineering Photonic Structures based on Nanoporous Anodic Alumina. Laura. K Acosta, Elisabet Xifre-Perez, Josep Ferré-Borrull, and Lluis F. Marsal. <u>Poster</u>
- SPPM 2021. Engineering of Photonic Structures in Nanoporous Anodic Alumina. Laura. K Acosta, Josep Ferré-Borrull, and Lluis F. Marsal. Poster
- 19. Conferencia Española de Nanofotónica (CEN) 2021. Nanoporous Anodic Alumina Photonic Crystals by Gaussian-Like Pulse Anodization. Laura K. Acosta, Elisabet Xifré-Pérez, Josep Ferré-Borrull, Abel Santos, Lluis F. Marsal. <u>Flash talk</u>

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> "Nothing in life is to be feared, it is only to be understood. Now is the time to understand more, so that we can fear less."

> > -Marie Curie-

Para Damián

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## Chapter 1. Introduction

#### 1.1 Background

NAA-PSs demonstrate considerable ability as advanced and useful optical sensing platforms due to their exceptional physical, chemical, and optical properties. The geometric properties of nanopores in NAA-PSs can be precisely engineered by different anodization approaches to selectively filter molecules by size-exclusion and increase the available binding functional sites due to the high specific surface area to volume ratio of these nanoporous PSs. Furthermore, the surface chemistry of NAA-PSs can be adjusted with different functional molecules. NAA-PSs are active optical platforms that confine, guide, reflect, emit, and transmit incident light, generating stable optical signals for optical sensing based on different spectral shifts upon exposure to analyte molecules such as transmittance. photoluminescence, reflectivity, waveguiding, absorbance, or color changes. Different forms of NAA-PSs such as distributed Bragg reflectors, grading-index filters, optical microcavities, Fabry-Pérot interferometers can be integrated with various optical techniques such as reflectometric interference spectroscopy (RIfS), reflection and transmission spectroscopy, and photoluminescence spectroscopy (PL). Recent progress in anodization technology has focused on structural engineering of NAA-PSs by distinct forms of pulse-like anodization approaches such as sinusoidal, sawtooth, pseudostepwise, and stepwise. In contrast to pioneering pulse-like anodization combining hybrid pulses between mild and hard anodization regimes, pulse anodization performed under mild conditions moderate electrolyte temperature and anodizing voltage/current density- provide superior controllability over the anodic oxide growth rate and its porosity. Despite these advances, to date only a limited number of pulse shapes have been implemented into anodization approaches to engineering distinct forms of NAA-PSs including sinusoidal, symmetric and asymmetric stepwise, and sawtooth. Although these strategies have successfully realized the engineering of NAA-PSs with outstanding optical properties, further developments of anodization technology will be needed to tailor-engineer the structure of NAA-PSs with versatility for harnessing specific forms of light-matter interactions and spreading the applicability of these unique photonic structures across light-based technologies.

#### 1.2 Motivation

Motivated by the previous works and the potential of these photonic structures of several applications like sensing, optical encoding, photonics, and photovoltaics. For this reason, this thesis is focused on the fabrication, characterization of Photonic Structures based in nanoporous anodic alumina using different anodization approaches. The obtained Photonic structures were tested as an optical sensing platform.

#### 1.3 Aims of the thesis

The objectives of this PhD thesis are the following:

- I. To improve and develop different nanoporous anodic alumina photonic structures.
- II. To fabricate nanoporous anodic alumina photonic structures with sinusoidal anodization profile.
- III. To fabricate new and advanced nanoporous anodic alumina photonic structures using several anodization approaches.
- IV. To apply these nanoporous photonic structures as an optical sensor.

# Chapter 2. Basis of Nanoporous Anodic Alumina (NAA)

UNIVERSITAT ROVIRA I VIRGILI ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla

# 2.1 Background of Nanoporous Anodic Alumina

#### 2.1.1 TimeLine of Nanoporous Anodic Alumina.

Nanoporous anodic alumina (NAA) is a self-ordered form of anodic aluminum oxide (AAO). Therefore, it is important to understand the chronological advances related with the engineering of pioneer structures of AAO. Anodized aluminum oxide has been used for the first time in the 20th century with protective and decorative purposes. In 1923, Bengough and Stuart patented a chromic acid-based electrochemical method for protecting aluminum from corrosion<sup>1</sup>. In 1927 the first anodization based on sulfuric acid was patented by Gower and O'Brien<sup>2</sup>. Afterwards, in 1936 Carboni patented a coloring method for aluminum foils by combination of an anodization step in sulfuric acid followed by a second step consisting of the application of alternating current in a metal salt solution<sup>3</sup>. Recently, thanks to the electron microscope invention, in 1953 Keller and coworkers characterized for the first time the honeycomb structure of AAO in the nanometric range, i.e., NAA and placed the groundwork for further NAA studies<sup>4</sup>. Based on this work and taking advantage of new techniques as microtome and electron microscope, Thompson and Wood published several studies providing a deep understanding in the growth mechanisms of aluminum oxide layers and a better knowledge of the anion incorporation and water content in the NAA structure<sup>5-9</sup>.

In 1995 Masuda et al. discovered how to fabricate porous alumina whit highly ordered pores by using a two-step anodization process<sup>10-11</sup>. They developed a cheap and highly reproducible strategy of fabrication which permits further studies of NAA in many laboratories. In 2002 Nielsch et al.

published an optimization of this procedure employing sulfuric, oxalic and phosphoric acid as electrolytes. After that many different types of anodization techniques have been established<sup>12-15</sup>. Two different forms of AAO with different morphology are obtained, depending on the electrolytes used for the anodization process. Commonly, with neutral acids (e.g., borate, oxalate...) nonporous-type membranes are formed<sup>16</sup> and with acidic electrolytes (e.g., sulfuric, oxalic, phosphoric...) porous-type membranes are formed. Nonporous AAO membrane is a compact oxide membrane also called barrier-type oxide or barrier layer. Porous AAO membranes consist in a porous membrane with pore sizes within the nanometric scale, also called Nanoporous Anodic Alumina (NAA)<sup>17</sup>.

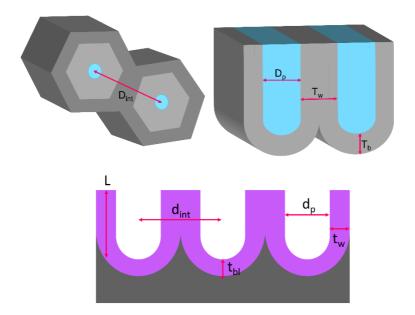
#### 2.1.2 Nanoporous anodic alumina Structure

Nanoporous Anodic Alumina is a honeycomb-like structure in which the hexagon is the unit cell, NAA is formed by several hexagonal cells. Each unit cell includes three different parts:

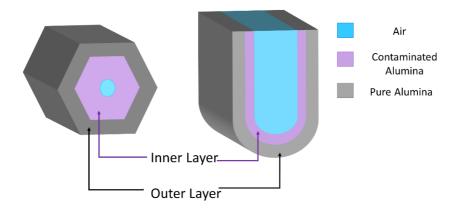
- i. The skeleton, a hexagonal inner layer which is produced of the common internal walls between the unit cells. The inner layer is composed of pure  $Al_2O_3$
- ii. An outer layer between the central pores. the outer layer is composed of  $Al_2O_3$  contaminated with impurities (anionic species i.e., phosphate, sulphate, oxalate, etc.) from the electrolyte.
- iii. The interstitial rod inside the inner layer at the triple cell junction.

The pore structural parameters are classified six different parts that includes (i) interpore distance ( $D_{int}$ ), (ii) pore diameter ( $D_p$ ), (iii) barrier layer thickness ( $T_b$ ), (iv) pore wall thickness ( $T_w$ ), (v) pore density ( $\rho_p$ ) and (vi) porosity ( $\rho$ )  $^{4,5,14-18}$ .

**Figure 2.1** a) shows schematically an idealized NAA honeycomb-like structure and its parts. **Figure 2.1** b) shows the main parameters which describe NAA structure. The thickness ratio of inner and outer layers (ri/o) depends on the electrolyte in the order: sulfuric acid ( $H_2SO_4$ ) < oxalic acid ( $H_2C_2O_4$ ) < phosphoric acid ( $H_3PO_4$ ) < chromic acid ( $H_2CrO_4$ )<sup>19</sup>. Also, Han *et al.* demonstrated that the anionic impurities incorporated depend on the anodization time and the electrolyte concentration<sup>20</sup>. They reported that electrolyte concentration decreases along the pore, so the contaminated area will be thicker on the top of the pores. Besides, one important property of these layers is that the outer layer is less resistant to chemical etching than the inner layer, which prevents the structure from collapsing even at high porosity. **Figure 2.2** shows the top and cross-sectional views of NAA pore showing the chemical composition distribution inside the nanopore walls.



**Figure 2.1** Schematic illustration of the NAA Honeycomb structure and its parts (a) honeycomb-like structure (b) Parameters describing the NAA structure.

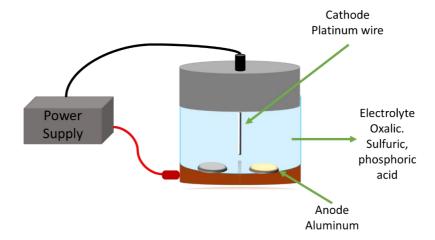


**Figure 2.2.** Schematic diagram of a nanoporous anodic alumina pore showing the chemical composition distribution inside the pore walls (top and cross-section).

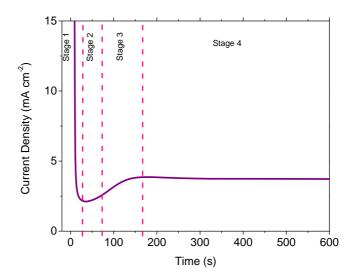
## 2.1.3 Electrochemistry process of Nanoporous Anodic Alumina

The same as other metals, when aluminum is exposed to air or water is spontaneously oxidized and a thin layer of aluminum oxide is formed over the surface. This thin layer protects the aluminum below from oxidizing more (natural protective layer). Nanoporous anodic alumina is formed by electrochemical oxidation of aluminum by an anodization process. Figure **2.3** shows the typical electrochemical cell used in the formation of NAA. NAA films are obtained by applying a direct voltage (U) through an electrolytic mixture (aqueous solution of acid, e.g., H<sub>2</sub>SO<sub>4</sub>, H<sub>2</sub>C<sub>2</sub>O<sub>4</sub> and H<sub>3</sub>PO<sub>4</sub>) into the aluminum substrate. Aluminum is used as an anode and usually a platinum or graphite is used as the cathode (while a material not affected by the electrochemical process). The applied voltage generates a high electric field (E) through the thin oxide layer on the surface of aluminum (natural protective layer). Under the electric field the anions of the solution (O<sup>2-</sup> and OH) travel to the anode in which aluminum is positively charged with resultant electrons lost. When a voltage is applied among the cathode and anode, pores nucleated and start to grow on the

aluminum surface. NAA membranes are generally formed under constant voltage or constant current density (J) conditions. Under a constant voltage, a usual anodization J versus time (t) curve can be divided into four NAA growth stages (figure 2.4)<sup>21-25</sup>.



**Figure 2.3** Schematic of Anodization system. Aluminum foil is used as anode and platinum as cathode. The anode and cathode are immersed in the acid electrolyte (oxalic, sulfuric, phosphoric or others) and all the system is linked to a power supply.



**Figure 2.4** Current density (J) versus time (S) during the porous AAO membrane formation divided in four stages. 1) The film of aluminum oxide starts to grow and forms a compact barrier layer, 2) Pores start to grow, 3) The anodizing process continues and 4) Arrangement of pores occurs and continue to grow.

**Stage 1**. Barrier layer creation. At the moment that is applying a constant voltage, the (J) will reach a high value quickly, that can be attributed to the existence of electrolytic process of water. A thin layer of aluminum oxide starts to grow on the surface of aluminum and creates a compact barrier layer that grows until a specific thickness. While the resistance of the barrier layer is proportional to its thickness, the current density decreases fast until the lowest value.

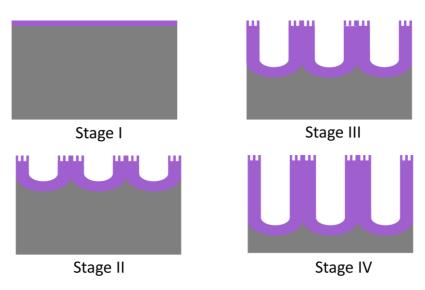
**Stage 2**. Pores growth. At the minimum value of current density (J) point, the electric field (E) concentrates on local defects or impurities on the growing aluminum oxide surface to create routes for electrolyte infiltration, which act as pore nucleation sites. Local field enhancement at the saturation routes facilitates oxide decomposition and leads to the formation of further pores.

**Stage 3**. Gradual increment in the current density (J). The pores continue to form thanks to the easy diffusion of the electrolyte inside pores that is possible due to the advanced anodization process. Finally, an equilibrium between the forming and dissolving aluminum oxide is reached and start stage 4.

**Stage 4.** Current density (J) achieves a steady-state. During this state, gradual reordering of pores occurs over time until the field (E) is the same for all the pores.

**Figure 2.5.** shows the schematics of the four NAA growth stages. The growth mechanism in stage 4 (steady-state) is the consequence of competing oxidation i.e., alumina formation at the aluminum-oxide

interface (in the inner layer) and the alumina dissolution at the oxideelectrolyte interface (in the outer layer) during the anodization process. Some possible reactions that are probably taking place have been reported.<sup>35-40</sup>



**Figure 2.5**. Schematic of NAA growth process under constant voltage condition. **I** to **IV** Morphology development with anodization time increasing.

Oxidation-reduction reaction that takes place during the anodization, it is the sum of the separate reactions at each electrode. **(Equation 2.1).** 

$$2Al_{(s)} + 3H_2O_{(l)} \rightarrow Al_2O_{3(s)} + 3H_{2(g)}$$
 (2.1)

The process begins with the heterolytic dissociation of water, (Equation 2.2).

$$2H_2O_{(l)} \rightarrow O_{(ox)}^{2-} + OH_{(ox)}^{-} + 3H_{(aa)}^{+}$$
 (2.2)

The  $O^{2-}$  and  $OH^-$  anions, under the influence of the electric field (*E*), leave the oxide-electrolyte interface (outer layer) and migrate through the barrier layer until the aluminium-oxide interface (inner layer). When  $O^{2-}$ 

comes at the aluminium-oxide interface, the metallic aluminium is oxidized and creates  $Al_2O_3$  (equation 2.3).

$$Al_{(s)}^{0} \to Al_{(ox)}^{3+} + 3e^{-}$$
 (2.3)

The ionic transport of  $Al^{3+}$  and  $O^2$  (equation 2.4) at the anode is exemplified in a schematic diagram in figure 2.6.

$$2Al_{(ox)}^{3+} + 3O_{(ox)}^{2-} \rightarrow Al_2O_{3(s)}$$
 (2.4)

 $H^+$  in contact with  $e^-$  released from the dissociation of water forms  $H_2$  (equation 2.5).

$$6H_{(ag)}^+ + 6e^- \rightarrow 3H_{2(g)}$$
 (2.5)

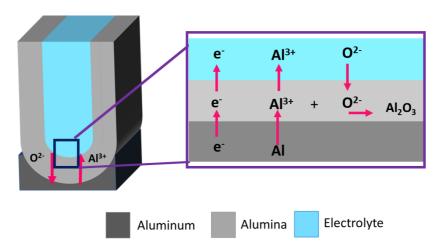


Figure 2.6. Schematics showing the ionic transport of  $Al^{3+}$  and  $O^2$ .

# 2.1.4 Anodization Techniques

Anodic Aluminum Oxide (AAO) membranes are fabricated using different anodization methods which leads the creation of AAO with specific characteristics. In this section we will describe the mild (MA) and hard anodization (HA).

#### 2.1.4.1 Mild Anodization

In 1995 Masuda and Fukuda publish by the first time the two-step method that allow the manufacturing of self-ordered AAO<sup>10-11</sup>. They observed that after long anodization process, the pores of the bottom start to be ordered in hexagonal arrays becoming a perfect ordered nanoporous structure and they proposed the two-step anodization method (**Figure 2.7**):

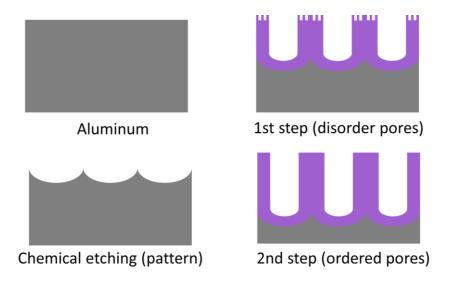


Figure 2.7 Schematics of the two-step anodization process.

- 1) The first anodization step results in a AAO membrane with disordered pores at the top but with ordered pores at the bottom.
- 2) After the first anodization step, the NAA membrane is removed and results in an aluminum surface with a honeycomb pattern of concavities.
- 3) The second anodization step will start to nucleate and grow the pores in a hexagonal ordered way. This procedure is characterized by anodization at low potentials and slow formation of pores due to the

low current density (J). With this technique is possible to obtain uniform pore size ( $D_p$ ) and interpore distance ( $D_{int}$ ) that can be easily tuned by selection of appropriate anodization conditions<sup>21</sup>.

# 2.1.4.2. Hard Anodization (HA)

This anodization method consists in the use of high voltages above the breakdown potentials. For a given anodizing electrolyte, there is a breakdown potential (U<sub>B</sub>) value (27 V for sulfuric acid, 50 V for oxalic acid and 197 V for phosphoric acid)<sup>22-24</sup> above which stable anodization is difficult to maintain due to the disastrous local current flow and consequent Joule heating which produces local burning and cracking in the growing<sup>21</sup>. This anodization produces NAA films faster and with a higher porous anodic layer growth rate than using MA<sup>25</sup>. Nevertheless, the substrate can be damaged because of the high voltage used. For this reason, HA is not typically used for nanotechnology research because it is difficult to properly maintain the anodization over the breakdown potential<sup>26-29</sup>.

# 2.1.5 Anodization parameters and Geometrical characteristics

The Nanoporous Anodic alumina (NAA) structure is especially different depending on the anodization parameters. Adjusting these specific parameters, it is possible tune the organized NAA structure easily. The anodization parameters which control the structural characteristics of NAA are the anodization voltage (U), anodization time (t) and temperature (T). Additionally, the particular characteristics of the electrolyte have an important effect in the NAA structure<sup>30-39</sup>.

#### 2.1.5.1 Anodization Temperature

The electrolyte temperature (T) affects the pore growth rate and pore diameter. High temperatures lead not only to faster growth rates but also high dissolution rate of formed oxide which promotes larger pores. (T) is a critical parameter due to during the anodization process an increment of temperature is probable to take place because of local heating<sup>26-27</sup>. This temperature increment can result in the fast dissolution of the pore walls due to the burning phenomenon. Moreover, the pore growth rate and pore diameter are affected by this parameter, decrease as T is reduced.

#### 2.1.5.2 Anodization Voltage

Flectrolyte

The pore diameter ( $D_p$ ) and interpore distance ( $D_{int}$ ) can be varied mostly by changing the anodization voltage (U)<sup>5,10-11,28-30</sup>. For a given electrolyte, there is a specific voltage (U), above which the breakdown and burning of NAA is most likely to occur due to the electron avalanche phenomenon. This phenomenon occurs due to local heating, increasing in the conductivity and ionization of atoms that leads excessive electron generation. **Table 2.1** shows the typically used electrolytes with their respectively used voltages<sup>40-41</sup>.

**Table 2.1**. Electrolyte voltage commonly used during the anodization process.

Voltage [V]

Licetiolyte	voitage [v]		
Sulfuric acid (H <sub>2</sub> SO <sub>4</sub> )	20		
Oxalic acid (H <sub>2</sub> C <sub>2</sub> O <sub>4</sub> )	40		
Phosphoric acid (H <sub>3</sub> PO <sub>4</sub> )	195		

#### 2.1.5.3 Electrolyte

One of the most important parameters for the fabrication of NAA films is the electrolyte composition. Moreover, the usual acid electrolytes used for fabricating NAA sulfuric, oxalic and phosphoric acid as was mentioned in Table 2.1, though other acids such as tartaric and malonic can be used to obtain NAA with particular characteristics<sup>45-46</sup>. The pH and viscosity of the acid electrolyte strongly affect the structural characteristics of the NAA: a) The pH influences mainly the pore diameter. Low pH values require low anodization voltages, that implicates a reduction of the dissolution of alumina which causes smaller pores. So, the pores are wider with H<sub>3</sub>PO<sub>4</sub> and narrower with H<sub>2</sub>SO<sub>4</sub><sup>47</sup>. b) The viscosity of the electrolyte affects directly on the final nanostructure. The increment of the viscosity produces a decrement on the current density during the anodization process. This current density reduction generates a decrement of the growth rate but also prevents the localized heating due to the reduction of the Joule effect. High viscosity helps to avoid oxide breakdown specially a high electric field<sup>48</sup>.

# 2.1.5.4 Interpore Distance (D<sub>int</sub>)and Pore Diameter (D<sub>p</sub>)

The interpore distance ( $D_{int}$ ) is the average distance between the centers of two adjacent pores. And the pore diameter  $D_p$  is the size radius of the pores. The interpore distance ( $D_{int}$ ) can be controlled precisely by voltage (U) (2.6) and is directly correlated with the pore diameter  $D_p$  (2.7). Pore diameter ( $D_p$ ) depends on voltage (U) but also depends on the temperature (T)<sup>20</sup>. The larger these parameters are, the bigger the pore diameter is. The pore sizes obtained by MA can vary between 10 to 400

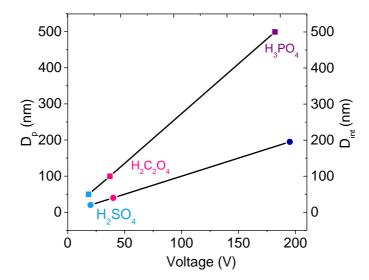
nm<sup>49</sup>. The relationship between the interpore distance and the anodization potential can be expressed as:

$$D_{int} = KU ag{2.6}$$

Where D<sub>int</sub> is the interpore distance, U is the anodization voltage and K is the proportionally constant whose value is between 2.5 and 2.8 nm V<sup>-1</sup> for Mild Anodization. Additionally, the relationship between the interpore distance, the pore diameter and the pore wall thickness can be expressed as:

$$D_{int} = D_p + t_w \tag{2.7}$$

Where, Dint is the interpore distance,  $D_p$  is the pore diameter and  $t_w$  is the wall thickness. Figure 2.8 shows the relationship between the  $D_p$  and  $D_{int}$  with the voltage and Table 2.2 shows the most usual anodization parameters for the three acid electrolytes generally used for MA. In addition, the average values of the resulting geometric characteristic are included.



**Figure 2.8**. Relationship between the geometrical characteristics  $D_p$  and  $D_{int}$  vs Voltage.  $D_p$  vs U (circles) and  $D_{int}$  vs U (squares). For each anodization electrolyte.

**Table 2.2** Summary of the usual anodization parameters and the geometric characteristics for sulfuric, oxalic, and phosphoric acid.

	H <sub>2</sub> SO <sub>4</sub>	$H_2C_2O_4$	H <sub>3</sub> PO <sub>4</sub>
Voltage [V]	20	40	195
Temperature [°C]	5	5	-5
Concentration	0.3 M	0.3 M	1% wt.
Pore diameter [nm]	20	40	195
Interpore distance [nm]	50	100	500

# 2.1.5.5 Porosity and Pore Density

The ratio of surface occupied by the pores to the total surface of the sample can be defined as porosity (P). Under Mild Anodization conditions, porosity follows the 10% porosity rule and usually is always about 10%<sup>50</sup> and under hard anodization conditions, this value is reduced to 3,3%<sup>51</sup>. The porosity can be correlated with pore diameter and interpore distance by the following equation:

$$P(\%) = \left(\frac{\pi}{2\sqrt{3}}\right) \left(\frac{D_p}{D_{int}}\right) * 100$$
 (2.8)

Where P (%) is the porosity,  $D_p$  is the pore diameter and Dint is the interpore distance in nanometers. The pore density is the number of pores that can be found on a specific area. The relationship between pore density and interpore distance can be expressed by the following equation:

$$\rho_p = \left(\frac{2}{\sqrt{3 D_{int}^2}}\right) * 100 \tag{2.9}$$

where  $(p_p)$  is the pore density, and  $D_{int}$  is the interpore distance.

#### 2.1.5.6 Barrier Layer Thickness

The barrier layer thickness (tb) is directly proportional to the anodization voltage (U) and is inversely proportional to current density (J). This relationship can be expressed as follows:

$$t_b = KU ag{2.10}$$

Where  $(t_b)$  is the barrier layer thickness value, K is a proportionally constant which depends on the anodization regime (1,3 nm/V for MA), and U is the voltage.

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UNIVERSITAT ROVIRA I VIRGILI

ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla

# Chapter 3. Fundamentals of Nanoporous Anodic Alumina Photonic Structures

UNIVERSITAT ROVIRA I VIRGILI ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla This Chapter presents the fundamentals of Photonic structures based on Nanoporous Anodic Alumina. The main concepts, different kind of photonic structures and the potential application of this structures are reviewed.

# 3.1 Background of Nanoporous Anodic Alumina Photonic Structures

In chapter 2 was explained the structure, fabrication and the design parameters of Nanoporous Anodic Alumina. The optical properties of NAA are very suitable for the formation of Photonic structures. The most attractive property of NAA is its versatile and highly controllable nanoporous structure, which can be readily utilized as an effective medium platform develop unique Photonic structures to modulate and control the flow of electromagnetic waves with precision. Nanoporous anodic alumina (NAA) produced by electrochemical oxidation of aluminum offers a set of unique properties that make it a highly attractive platform material for the fabrication of PSs. These include scalable and cost-effective fabrication process, highly controllable self-organized nanoporous structure based on well-defined cylindrical nanopores of high aspect ratio, chemical resistance, thermal stability, mechanical robustness, and optical properties. 1-2 NAA is considerate as a base material for the development of PCs. Pioneering fundamental studies dealt with the development and assessment of 2D NAA-PSs featuring straight cylindrical nanopores from top to bottom.<sup>3-5</sup> These studies demonstrated that the optical properties of NAA-PCs can be tuned by the geometric features of its nanoporous structure and its chemical composition which can be controlled using different anodization

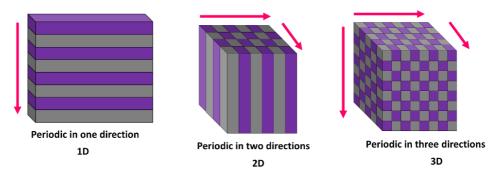
conditions.<sup>2</sup> The development of anodization approaches directing to modulate the nanoporous structure of NAA in depth opened new opportunities to create multi-dimensional (1D, 2D and 3D) NAA-Photonic Structures. Following these studies Choi et al. studied the reflection spectrum of 2D NAA-PSs in the NIR region and analyzed the effect of the filling factor (i.e., ratio pore radius/interpore distance) on the characteristic PSB.<sup>6</sup> An almost linear blue shift of the PSB position was observed when the nanopores of NAA were widened by wet chemical etching (i.e., increment of filling factor) under controlled conditions. These studies represent the first demonstration and utilization of NAA as a platform for the development of Photonic structures. Nevertheless, the versatility of these PSs to attain light control in the different regions of the spectrum is limited by the range of lattice constants (i.e., d<sub>int</sub>) in NAA. Another strategy to generate PC structures based on NAA is the in-depth modulation of its nanopores during anodization by structural engineering.

#### 3.2 Photonic Structures.

Photonic structures (PSs) are a class of optical nanostructures with allowed and forbidden photonic bands that modify the movement of photons by altering the dispersion of electromagnetic waves when photons travel across the structure of PS. These light–matter interactions can be tuned with accuracy by engineering the PCs' structure, which features regularly distributed regions of high and low refractive index in one, two, or three dimensions. Figure 3.1 shows the schematics of the three types of Photonic structures in one, two and three dimensions. Nanoporous PSs are particularly good structures to develop ultra-sensitive optical sensing platforms since they supply:

- a) Light-modifying capacities to alter and engineer the flow of photons at specific spectral regions from UV to IR.
- b) The nanoporous structure that facilitates the transport of molecular species involved in binding events.
- c) High specific surface area that increases the number of functional binding sites within the optical platform.<sup>10</sup>

Furthermore, PSs are a promising platform for other kinds of applications like photocatalysis, drug delivery, optical encoding, photovoltaics and others. **Figure 3.1** Schematics of three types of the photonic structures in one, two and three dimensions.



**Figure 3.1.** Schematics of the three kinds of photonics structures in one, two and three dimensions.

Nanoporous anodic alumina (NAA) is a promising material to developed PSs due to their unique optical properties. The optical properties of NAA rely intrinsically upon its nanoporous architecture. Therefore, to engineer the nanoporous structure of NAA provides novel means of modulating its refractive index in a multidimensional fashion to fabricate advanced materials with unique optical properties to guide, reflect, transmit, emit, and enhance incident light. The nanoporous structure of NAA can be engineered by means of different anodization approaches to produce PC structures with finely tuned optical properties across the spectral regions.

NAA provides controllable and versatile nanopore geometry, chemical and physical stability, stable and tunable optical signals, and mechanical strength. Furthermore, NAA's surface chemistry can be modified with a broad range of functional molecules to achieve chemical selectivity toward analytes of interest. 11-12 Structural engineering of the nanoporous structure of NAA in depth enables the generation of PC structures, the most representative examples of which are Fabry–Perót interferometers, distributed Bragg reflectors, gradient-index filters, apodised gradient index filters, microcavities, and optical bandpass filters.

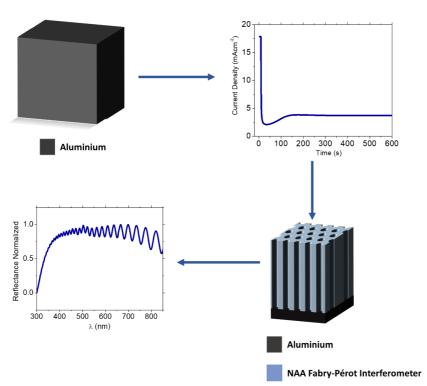
#### 3.2.1 Fabrication of Photonic Structures

The effective medium of NAA can be engineered in depth with precision during anodization in order to produce photonic structures of high aspect ratio with features of precise regularity and optimal resolution to diffract electromagnetic waves within the UV-visible-NIR spectrum. Even though NAA was used as a matrix for the development of photonic crystals. Recent anodization approaches have made it possible to overcome the intrinsic limitations of NAA fabrication, enabling a new path for the fabrication of a broad range of highly tunable photonic structures, which could open opportunities for all-optical NAA-based optical devices. 13-17 Pioneer studies by Masuda et. al and Gösele et. al revealed that organized NAA-PSs feature a characteristic photonic stopband (PSB) in their optical spectrum, the position of which can be finely tuned by the interpore distance (i.e., lattice constant—distance between the center of adjacent nanopores) and porosity (i.e., pore diameter) of the NAA-PC platform. Structural engineering of the nanoporous structure of NAA in depth enables the formation of PC structures, the most representative examples of which are Fabry–Pérot interferometers<sup>18-19</sup>, distributed Bragg reflectors<sup>20-22</sup>, gradient-index filters (Rugate Filters)<sup>23-25</sup>, microcavities<sup>26-27</sup>, and optical bandpass filters<sup>28</sup>. NAA–PSs, which can be produced with precision by pulse-like anodization strategies trying to engineer the effective medium of NAA.

#### 3.2.1.1. Fabry-Perot Interferometers

Fabry–Perot interferometers based on Nanoporous Anodic Alumina (NAA-FPIs) include a distribution of effective refractive index in depth and have been intensively used as sensing platforms in combination with different techniques. NAA-FPIs interfere constructively with electromagnetic waves, generating a characteristic interference pattern with distinctive fringes, which are a result of the Fabry–Pérot effect. Variations of the effective medium of NAA-FPIs leads to shifts in their typical interference pattern, which can be used as sensing principle to create optical systems with broad applicability<sup>18</sup>. The number, position, and intensity of these oscillations rely on the NAA thickness (i.e., the pore length (Lp)) and its porosity (i.e., the pore diameter (dp))<sup>29</sup>.

Therefore, this property offers us an excellent opportunity for designing NAA structures with tunable optical properties by modifying the pore geometry. The fabrication of this kind of structure follows the well-known two-step anodization process developed by Masuda and co-workers<sup>30</sup>. **Figure 3.2** shows the fabrication process used for the formation of Fabry-Pérot interferometer and the characteristic reflection spectrum of these kind of structures.

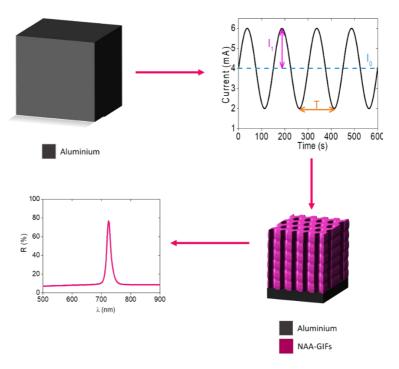


**Figure 3.2** Fabrication process of Fabry-Pérot structures by constant anodization. Showing straight pores. The reflection spectrum shows the characteristic optical oscillations.

#### 3.2.1.2 Gradient Index Filters

NAA-GIFs produced by sinusoidal pulse anodization feature a characteristically well-resolved, intense, and narrow PSB associated with a smooth and periodic modulation of the effective refractive index in depth, which is  $\sim \pi/4$  narrower than that of their quarter-wave NAA-DBR. Well-resolved and narrow PSBs are desirable for different light-based applications requiring a precise control over electromagnetic waves such as optical sensing and biosensing, optical encoding and photocatalysis. Recent developments in pulse anodization technology have aimed at improving the quality of light control of NAA-PCs. A variety of sinusoidal pulse anodization strategies have been explored to improve

the quality of light control in NAA-GIFs, including implementation of apodization functions into anodization profiles<sup>35</sup> and application of anodizing voltage as a function of optical path length.<sup>36</sup> NAA-GIFs produced by these and other approaches have achieved high quality PSBs, with quality factors. **Figure 3.3** shows the fabrication process of NAA-GIFs by sinusoidal pulse anodization and the representative reflection spectrum of the characteristic reflection bands.

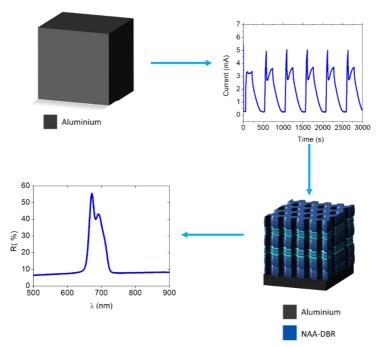


**Figure 3.3** Fabrication process of Nanoporous Anodic Alumina Gradient Index Filters using sinusoidal pulse anodization.

# 3.2.1.3. Distributed Bragg Reflectors (DBR)

The distributed Bragg reflector (DBR) is a multilayered structure that consists of periodically stacked layers with different refractive indexes. The main optical property of a DBR is that it can block light propagation in the direction perpendicular to the refractive index variation for a certain

wavelength range, called the stop band. <sup>22,37</sup> The central wavelength of this stop band depends on the refractive index and thickness of the layers composing the DBR, whereas the stopband width depends basically on the contrast between the refractive indexes and the relative thicknesses between the layers within one period, although it also depends on the total number of layers. DBRs are structures that can control the incident light (completely or partially) inside the material. This interesting photonic property makes DBRs potential candidates for the fabrication of various optoelectronic devices: light filters, <sup>38</sup> vertical cavity surface-emitting laser, <sup>39-40</sup> reflector mirrors, <sup>41</sup> electro absorptive reflection modulators, <sup>42</sup> and others. To obtain DBR structures exists different kind of anodization process like cycling anodization voltage<sup>22</sup> and current density pulse anodization <sup>43</sup>. Figure 3.4 shows the fabrication process of NAA-DBR using cycling anodization and the reflection spectrum of the obtained band.



**Figure 3.4**. Fabrication process of NAA-DBR by cyclic anodization and the reflection spectrum of the characteristic photonic band.

#### 3.2.1.4 Microcavities

The fabrication of Nanoporous Anodic alumina microcavities (NAA- $\mu$ CVs) involves the introduction of defect modes in the Photonic Structure, which can be achieved by various approaches such as the insertion of a thin layer of nanopores with constant effective refractive index between two highly reflective Bragg mirrors, a phase shift of the effective refractive index between Bragg mirrors, or a progressive asymmetric modulation of the effective medium in depth. However, the maximum quality factors of NAA- $\mu$ CVs reported by Wang et al. and Yan et al., Were found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be the low refractive index of alumina (Al<sub>2</sub>O<sub>3</sub>; n-Alumina  $\sim$  1.70). Here were found to be a significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than those of porous silicon-based  $\mu$ CVs are found to be significantly lower than the found to be significantly lower than the found to be significantly lower than the found to be signifi

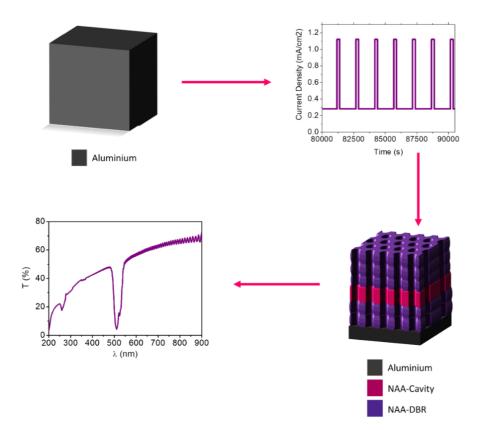
Despite this limitation, the development of new pulse-like anodization strategies and novel NAA-PC architectures provides new opportunities to improve the quality of NAA-μCVs and explore new strategies to attain strong light confinements by precise control of light–matter interactions at the nanoscale.<sup>27</sup> Recent studies identified sharp resonance bands within the photonic stopband (PSB) of NAA-PCs produced by stepwise pulse anodization when a logarithmic negative apodization function was applied under certain conditions.<sup>27,50-51</sup>

However, only a few studies have explored the potential of these emerging optical transducers as sensing platforms. Yan et al.,  $^{46}$  and Lee et al.,  $^{61}$  demonstrated that NAA– $\mu$ CVs are sensitive PC structures to changes in refractive index, while Wang et al. proved that NAA– $\mu$ CVs' RB undergoes dynamic spectral shifts upon exposure to humidity from water vapor. Despite these advances, there remain fundamental questions concerning the design and engineering of NAA– $\mu$ CVs to maximizing

sensitivity of light confined within their structure for practical sensing applications. Previous studies on nanoporous  $PCs^{63-64}$  point that sensitivity of NAA– $\mu$ CVs is critically determined by:

- a) size of analyte molecules,
- b) degree to which analyte molecules increase the refractive index of the medium filling the nanopores
- c) molecule-surface interaction strength
- d) spectral position and quality of light confinement.

Figure 3.5 shows the fabrication process of NAA- $\mu$ CVs by stepwise pulse anodization and the reflection spectrum showing the NAA- $\mu$ CV.



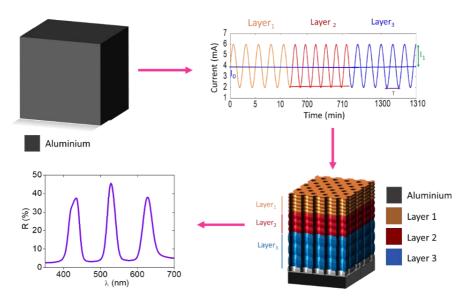
**Figure 3.5**. Fabrication process of optical microcavities NAA-μCvs.

#### 3.2.2 Multispectral Photonic Structures

To fabricate PCs with multiple narrow photonic stopbands at different spectral positions remains challenging, and to date, only a few proof-of-concept studies have realized this class of PCs. For instance, Sailor et al., 52,53 and Santos et al., 54 developed porous silicon and NAA-PC structures, respectively, with multiple photonic stopbands at different spectral positions. These PCs were obtained by averaging the sum of multiple sinusoidal waves into a single complex waveform, which was subsequently translated into anodization profiles to engineer the nanoporous structure of these PCs in depth. Each sinusoidal wave determines the position and the reflectance amplitude of a forbidden photonic band or photonic stopband.

Multiple-band NAA structures have interesting applications such as optical encoding, optical sensing, photonics and photovoltaics. 55-60 However, the average sum of multiple sinusoidal waves and their implementation into anodization processes that are effectively translated into modulations of effective refractive index present some limiting drawbacks. When the number of forbidden bands is increased, the reflectance amplitude of each band is reduced. The reflectance amplitude of each forbidden band is proportional to the amplitude of the sinusoidal wave. Therefore, when the number of bands increases, the multiple averaging reduces the amplitude of each sinusoidal wave proportionally to the number of bands, thus decreasing the reflectance amplitude of all the bands in the spectrum of these PCs. **Figure 3.6** shows the fabrication process of the NAA- multispectral-PSs, the anodization profile shows a part of the current process of each layer. The reflection spectra show

three photonic sop bands corresponding with each layer fabricated. This anodization approach is very useful for the formation of sensing platforms, drug delivery systems, optical encoding, photocatalysis, band pass filters and others.



**Figure 3.6.** Fabrication process of NAA-multispectral-PSs. The reflection spectrum shows three PSB corresponding with the three stacked layers.

#### 3.2.2.1. Optical Bandpass Filters

Optical bandpass filters (BPFs) are photonic structures that allow the transmission of a specific portion of the light spectrum in a selective manner while impeding the passing of light of all other wavelengths.<sup>65</sup> BPFs are extensively used across a broad range of disciplines and industries, including photography, astronomy, the pharmaceutical industry, medicine, physics, and chemistry. Generally, BPFs are classified into three categories according to the range of allowed wavelengths:

- a) long-pass filters, which allow the transmission of light of long wavelengths,
- b) short-pass filters, which allow the passing of light of short wavelengths,
- c) bandpass filters, which allow the transmission of a band of wavelengths while blocking the passing of light of shorter and longer wavelengths.

The first obtained Bandpass filters based on nanoporous anodic alumina (NAA-BPF) were carried out by Santos and Co-workers. Bandpass filters (NAA–BPFs) produced by a pseudo-stepwise asymmetric pulse anodization approach under galvanostatic conditions in sulfuric acid electrolyte at low temperature. <sup>66</sup> The anodization approach was based on asymmetric stepwise current density pulses. The effect of the anodization period over the position and FWHM of the PSB of NAA–BPFs was first established. Using this rationale, the combination of stacked NAA–BPFs produced with different anodization periods can be readily used to create different transmission bands at specific positions across the transmission spectrum of the PC heterostructures. Besides, the progressive modification of the anodization period in the stacked NAA–BPF structure can be used to engineer the width of the PSB.

**Table 3.1** shows a compilation of anodization approaches for the formation of the most characteristic photonic structures. This table includes the references of the principal studies involved in this anodization approaches.

**Table 3.1** Summary of the main anodization approaches.

Photonic Structure	Anodization approach	Reference	
NAA-FPI	One step anodization	3-5	
INAA-FPI	Two-step anodization	67,76-78,112	
NAA-GIFs	Sinusoidal pulse anodization	24-25,32	
NAA-GIFS	Pseudo-stepwise pulse anodization	83-84	
NAA-DBR	Stepwise pulse anodization	20,26-27,43-46	
	Pseudo stepwise pulse anodization	50,76,89,113	
NAA-μCVs	Stepwise pulse anodization	26	
	Sinusoidal pulse anodization	27	
	Pseudostepwise pulse anodization	44-46	
	Sawtoth pulse anodization	89	
NAA-BPF	Stepwise pulse anodization	28	
	Pseudo stepwise anodization		
	Stepwise pulse anodization + sinusoidal		
	pulse anodization		
NAA-multispectral-PS	Sinusoidal Pulse anodization	91, 119	

# 3.3 Potential Applications of Nanoporous Anodic Alumina Photonic Structures

The promising optical properties of NAA-PSs make it an innovative platform. Since the first pioneering works NAA-PS have been used as platforms for optical sensors<sup>67-72</sup>, recently they have also been used for photocatalysis<sup>90</sup>, drug delivery<sup>91</sup>, optical encoding<sup>34</sup>, photovoltaics and lasing systems.

## 3.3.1 Optical sensors

Optical sensors are devices that use different kinds of light–matter interactions to detect and quantify molecules for multiple applications. They contain a light source to generate electromagnetic signals, a sensing platform in which light–matter interactions appear, and a detector to identify and quantify spectral shifts in electromagnetic waves upon interaction and exposure to analytes.<sup>73-75</sup> Usually, the sensing principle in optical sensors depend on shifts in the characteristic spectral property of

the optical platform upon interaction with molecules. NAA-PSs show much potential as advanced and versatile optical sensing platforms due to their excellent physical, chemical, and optical properties. To engineer the effective medium and surface chemistry of NAA-PSs enhances the sensing performance and capabilities of NAA-based optical sensing system in terms of selectivity, sensitivity, and specificity. The geometric features of nanopores in NAA-PSs can be precisely engineered by different anodization approaches to selectively filter molecules by size-exclusion and increase the available binding functional sites due to the high specific surface area to volume ratio of these nanoporous PSs.

NAA-PSs are active optical platforms that confine, guide, reflect, emit, and transmit incident light, generating stable optical signals for sensing applications based on different spectral shifts upon exposure to analyte molecules such as reflectivity, photoluminescence, transmittance, waveguiding, absorbance, or color changes. Recent research advances in NAA-PSs as an optical sensing platform demonstrated that the NAA-PSs are an excellent platform due to their high controllable and tune the effective medium and versatile surface chemistry, which can be precisely engineering to achieve performance for an extensive molecules and analytes. Several researches are focus on the fabrication of photonic structures for develop optical sensor systems showing selectivity, sensitivity and Low Limit of detection.

**Table 3.2** shows a compilation of the recent sensing performances for the different Photonic structure. All of these studies demonstrated the ability of the NAA-PSs structures for been used as optical sensing platforms for a broad range of analytes.

**Table 3.2** Recent sensing performances for different photonic structures (NAA-PSs)

Photonic Structure	Analyte	Reference		
	D-Glucose	76		
	Proteinase K	77		
	Hg	76		
Folomo Démod	Gold iones	19, 78		
Fabry Pérot Interferometeres	Cancer cells	79		
	TNF	80		
	Cysteine	67		
	Trypsin	81		
	Galactosidase	82		
	D-Glucose	32		
	Indomethacin	25		
	HSA	83		
	Salicylic acid	83		
GIFs	Metal ions (Hg, Cu, Pb)	84		
GIFS	Ethanol	24		
	Alcohols mixtures	24		
	Sulfadymethoxine	85		
	Warfarin	85		
	Coumarin	85		
	D-Glucose	87		
	Ethanol-IPA	43,87		
	Gold Iones	87		
DBR	Vitamin C	43		
DBK	Hg	43		
	Alkanes	87,88		
	Organic molecules	88		
	Au	87		
	Humidity sensor	45		
	gas sensor	46		
Ontical microsovities	Alcohols mixture	89, 27		
Optical microcavities	Hexane	89		
	Nacl	27		
	Au ions	43		

## 3.3.2 Photocatalysis

Photocatalysis is a light process in which photons interact with atoms (matter–semiconductor) to generate electron–hole pairs that produce free radicals able to undertake secondary reactions. Photocatalytic processes involve a photoactive material (e.g., semiconductor, noble

metal) with a well-defined energy bandgap<sup>91</sup>. When the energy of the incoming photons is higher than the energy bandgap of the platform material, electrons and holes are generated in the materials conduction and valence bands, respectively.

Typical photocatalyst materials have fundamental constraints such as low photon-to-electron conversion rates due to limited utilization of highirradiance solar spectral zones and low effective surface area<sup>91</sup>. The efficiency of photocatalysts system can be improved by engineering their structure at the nanoscale in the form of nanoporous photonic structures (PSs), which provide high specific surface area, improved utilization of incoming photons, and efficient mass transport of ionic and molecular species involved in photocatalytic reactions<sup>94-97</sup>. Inverse opal PC photocatalysts feature a characteristic photonic stopband (PSB) that can be engineered with precision across the spectral regions to harvest incoming photons from high-irradiance spectral regions <sup>99-102</sup>. Although these PC structures have been explored as platform material for photocatalysis, they present several inherent drawbacks, including long fabrication process, restriction to 3D nanostructures, constraints to small domain areas and formation of structural defects<sup>103</sup>. Among other alternatives, electrochemically engineered nanoporous materials are promising photocatalyst platforms due to their versatile, highly controllable and self-organized nanoporous structure. Advances in electrochemical oxidation of aluminum and titanium enable new opportunities to precisely modulate and engineer the effective medium of semiconductor oxides to harness light-matter interactions for photocatalysis.

NAA-PSs such as gradient-index filters, optical microcavities, and distributed Bragg reflectors present as ideal platforms to utilize the "slow photon" effect for enhanced photocatalytic reactions. However, the wide energy band gap of NAA<sup>104, 105</sup> prevents the direct use of NAA-PSs for photocatalysis. Despite this intrinsic limitation, the chemical-modification of NAA-PSs with photoactive materials such as TiO<sub>2</sub> does provide an opportunity to develop new platform materials as highly efficient photocatalysts by a rational management of photons at the nanoscale

The research advances in nanoporous PSs have been demonstrated the ability of these structures to be efficient for photocatalysis systems. Santos and co-workers have been demonstrated the use of different photonic structures by photocatalysis system. **Table 3.3** summarize the most recent advances in photocatalysis using NAA-PSs this table includes the optical mechanism used in each study.

**Table 3.3.** Summary of the recent studies in photocatalysis with NAA-PSs.

Photonic structure	Optical mechanism	Reference
TiO <sub>2</sub> -NAA-GiFs	Slow photon	23
TiO <sub>2-</sub> NAA-DBR	Slow photon	98
TiO <sub>2</sub> -NAA-μQVs	Light recirculation	26
TiO2-NAA-BDBR	Slow photon	106
Au-TiO <sub>2</sub> -NAA-DBRs	Slow photon + surface	107
	plasmon resonance	

## 3.2.3 Drug delivery

In drug delivery advances, the release of the target molecule has been a major challenge; consequently, different stimuli are currently used to maintain the drug molecules and release them only when triggered by any specific stimulus. In this regards, pH-sensitive mechanisms draw huge

attention as they are similar to the pH variations inside the human body. From Now, polyelectrolyte multilayers (PEM) have been frequently used to cover the surface of nanoporous structures for the continued delivery of drug molecules 108-110. One of the principal problems when PEM are used in NAA nanostructures is the determination of the degree of drug loading into the pores and the rate of release of the drug-loaded into the nanostructure. Recently, was developed an optical platform based on Nanoporous Anodic Alumina Gradient Index filters (NAA-GIFs). The study developed by Kapruwan et. al demonstrates successfully the ability of these nanostructures for analyzing the loading and release of a cargo molecule. To achieve this, NAA-GIFs composed of two photonic stopbands have been obtained, infused with the cargo molecule, and monitored optically for their loading and releasing patterns. 111

### 3.3.4 Optical encoding

This innovative anodization approach, so-called multi-sinusoidal pulse anodization based on the combination of multiple sinusoidal waves into a single complex waveform, which corresponds to the average sum of several sinusoidal waves. This electrochemical nanofabrication method is demonstrated as a unique means of engineering the photonic stop band of nanoporous anodic alumina in depth. photonic structures based on Nanoporous Anodic Alumina can be used to encode information within their optical transmission spectrum. Santos et.al developed as a proof-of-concept, an 8-bit encoding system with ON (1)/OFF (0) states is for the first time implemented and demonstrated in NAA-based photonic structures, opening new opportunities for robust and reliable nanoscale platforms for secure information storage and optical encoding<sup>28</sup>.

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Chapter 4. Nanoporous Anodic
Alumina Photonic Structures
with Multi-Spectral Photonic
Bands

UNIVERSITAT ROVIRA I VIRGILI ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla This chapter presents the development and optical engineering of stacked nanoporous anodic alumina photonic structures with multispectral bands. (NAA-MPSs) with tunable multi-spectral photonic stopbands for sensing applications. The structure of these photonic crystal (PC) is formed by stacked layers of NAA produced with sinusoidally modified effective medium. The progressive modification of the sinusoidal period during the anodization process enables the generation and precise tuning of the characteristic photonic stopbands (PSB) (i.e., one per sinusoidal period in the anodization profile) of these PC structures.

#### 4.1 Introduction

The design and engineering of nanostructures with innovative architectures and materials can pave the way for controlling light-matter interactions at the nanoscale in novel ways. These nanostructures would enable new opportunities to develop advanced materials for a plethora of applications, including optical chemical and biosensing<sup>1–4</sup>, drug delivery<sup>5,6</sup>, and photonic encryption<sup>7</sup>. Photonic crystals (PCs) are a class of optical nanostructures with allowed and forbidden photonic bands that modify the movement of photons by altering the dispersion of electromagnetic waves when photons travel across de PC's structure.

PCs modulate the flow of light when photons travel across the material. These light-matter interactions can be tuned with accuracy by engineering the PC's structure, which features regularly distributed regions of high and low refractive index in one, two or three dimensions <sup>8–16</sup>. PCs can be produced with different architectures and materials to attain light modulation across the broad range of spectral regions (from UV to IR),

depending on the application needs <sup>17–22</sup>. Of all PC architectures, gradient index filters (GIFs) are PCs that are typically used as selective filters due to their narrow photonic band.<sup>23</sup> These photonic structures have also been explored as platforms to develop highly sensitive optical sensors.<sup>24</sup> When the effective medium of gradient-index filters is changed, the characteristic band undergoes spectral shifts that can be used as sensing principle for a variety of optical sensing systems.<sup>25</sup>

Nanoporous anodic alumina (NAA) is a promising base material for the fabrication of PCs. NAA is formed by the electrochemical oxidation (anodization) of aluminum, a cost-effective and fully scalable process compatible with conventional micro- and nanofabrication approaches that allows the precise control over the geometry and distribution of the pores<sup>26,27</sup>. The optical properties of NAA rely intrinsically upon its nanoporous architecture. Therefore, to engineer the nanoporous structure of NAA provides novel means of modulating its refractive index in a multi-dimensional fashion to fabricate advanced materials with unique optical properties to guide, reflect, transmit, emit, and enhance incidence light.<sup>28,29</sup>.

Furthermore, NAA has high chemical and physical stability, provides stable optical signals without further surface passivation and its surface chemistry can be easily modified with a broad range of functional molecules for multiple applications, including chemo- and biosensing, drug delivery, optical encoding, theranostics implants<sup>30,31</sup>, catalysis and electromagnetism<sup>32,33</sup>. NAA is particularly interesting for the development of optical sensing platforms since it is optically active (i.e., can alter the motion of photons in different ways) and its nanopores can work as

nanocontainers to accommodate analytes of interest. NAA can be modified with functional molecules to provide selectivity toward a broad range of analytes and its nanopore geometry can be engineered to increase the effective surface area for binding events. 34–43 To fabricate PCs with multiple narrow photonic stopbands at different spectral positions remains challenging and to date, only a few proof-of-concept studies have realized this class of PCs. For instance, Sailor et al 44,45, and Santos et al developed porous silicon and NAA-PC structures respectively with multiple photonic stopbands at different spectral positions.

These PCs were obtained by averaging the sum of multiple sinusoidal waves into a single complex waveform, which was subsequently translated into anodization profiles to engineer the nanoporous structure of these PCs in depth. Each sinusoidal wave determines the position and the reflectance amplitude of a forbidden photonic band or photonic stopband. Multiple-band NAA structures have interesting applications such as optical encoding tags, optical sensing, photonics and photovoltaics <sup>44,47–53</sup>. However, the average sum of multiple sinusoidal waves and their implementation into anodization processes that are effectively translated into modulations of effective refractive index present some limiting drawbacks. When the number of forbidden bands is increased, the reflectance amplitude of each band is reduced. The reflectance amplitude of each forbidden band is proportional to the amplitude of the sinusoidal wave.

Therefore, when the number of bands increases, the multiple averaging reduces the amplitude of each sinusoidal wave proportionally to the number of bands, thus decreasing the reflectance amplitude of all the

bands in the spectrum of these PCs. Therefore, this fabrication approach is amplitude-limited and do not offer enough controllability to generate multiple spectral forbidden bands with high intensity. To overcome this limitation, in this chapter we devise an alternative fabrication method that enables the production of NAA-based PCs featuring multiple forbidden bands at specific spectral positions with higher intensity. Multiple sinusoidal current density waveforms of different period are applied sequentially during anodization to produce composite NAA-PC structures composed of stacked NAA-MPSs. In contrast to previous methods using complex averaged waveforms, the sequential application of sinusoidal anodizing current density periods provides a suitable means of creating NAA-PCs with multiple forbidden bands with high intensity. The flexibility of this novel fabrication method to design and engineer the tunability of multi-spectral photonic stopband in these NAA-PCs is evaluated in realtime. The sensitivity of the effective medium of these PC structures upon changes of the medium filling the pores is systematically assessed to demonstrate the potential of these NAA-PCs as optical sensing platforms.

### 4.2 Experimental details

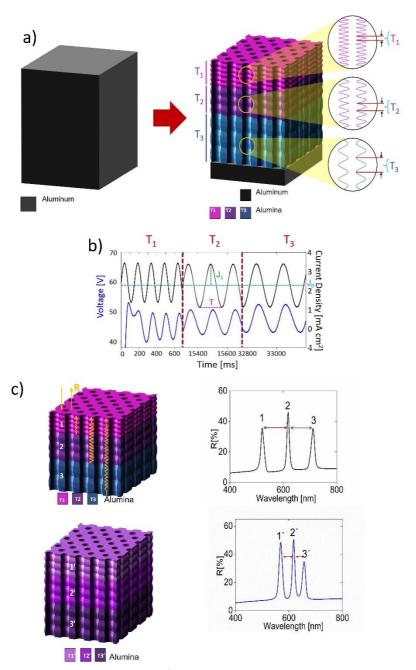
# **4.2.1** Fabrication of Photonic Structures with multi-spectral photonic bands (NAA-MPSs)

Aluminum substrates were cleaned with acetone, water, and ethanol in order to remove all the impurities and grease. Before anodization, aluminum substrates were electropolished in a solution 4:1 v/v of ethanol-perchloric acid at 20 V and 5°C for 6 min, with the stirring direction alternated every 60 s. Subsequently, anodization of aluminum substrates

was carried out in oxalic acid 0.3 M at 5°C by applying a current density—time anodization waveform that modulates the pore diameter in depth, as the NAA layer grows. Finally, the remaining aluminum was removed from the backside of the NAA-MPSs by chemical etching with a saturated solution of HCl and CuCl<sub>2</sub> for optical characterization. A set of anodization profiles were generated to produce NAA-MPSs with three forbidden bands positioned at specific wavelengths within the visible region of the spectrum following Equation 4.1.

$$J(t) \begin{cases} J_{1} \sin\left(\frac{2\pi}{T_{1}}t\right) + J_{0} & 0 \leq t < NT_{1} \\ J_{1} \sin\left(\frac{2\pi}{T_{2}}t\right) + J_{0} & NT_{1} \leq t < NT_{1} + NT_{2} \\ J_{1} \sin\left(\frac{2\pi}{T_{3}}t\right) + J_{0} & NT_{1} + NT_{2} \leq t < NT_{1} + NT_{2} + NT_{3} \end{cases}$$
(4.1)

where J(t) is the anodization current density at time t,  $J_1$  is the current density amplitude,  $T_i$  (i = 1, 2, 3) is the anodization period and  $J_0$  is the offset current density. For this purpose, the anodization current density waveform was formed by three sequential sinusoids with three different pulse periods (i.e.,  $T_1$ ,  $T_2$  and  $T_3$ ). The rest of the sinusoid parameters such as offset current density ( $J_0$ ), current density amplitude ( $J_1$ ) and number de periods (N) were kept constants for all the sinusoids. **Figure 4.1a** shows a conceptual illustration of the fabrication process used to generate multispectral NAA-MPSs including a representative anodization profile (**Figure 4.1b**) and schematics of the different layers composing the structure of NAA-MPSs with the corresponding anodization period and the reflection spectrum of a NAA-MPSs with  $J_0 = 2.6$  mAcm<sup>-2</sup>,  $J_1 = 1.3$  mAcm<sup>-2</sup>,  $J_1 = 150$ ,  $J_2 = 175$  and  $J_3 = 200$  s, and  $J_3 = 180$  s, and  $J_3 = 2.6$  mAcm<sup>-2</sup>,  $J_1 = 1.3$  mAcm<sup>-2</sup>,  $J_2 = 1.3$  mAcm<sup>-2</sup>,  $J_3 =$ 



**Figure 4.1.** Conceptual illustration of the electrochemical approach used to produce multi-spectral NAA-MPSs by sinusoidal current density profile for three photonic stopbands. (a) Fabrication process of multi-spectral NAA-MPSs. (b) Sinusoidal anodization profile of a representative multi-spectral NAA-MPS. (c) Schematics showing the existing relationship between nanoporous architecture and optical properties of multi-spectral NAA-MPSs for the samples produced with  $J_0=2.6~\text{mAcm}^{-2}$ ,  $J_1=1.3~\text{mAcm}^{-2}$ ,  $T_1=150$ ,  $T_2=175$  and  $T_3=200~\text{s}$ , and  $T_3=100~\text{periods}$ , and  $T_3=100~\text{c}$ .

**Table 4.1** summarizes the fabrication conditions of the different NAA-MPSs produced in this study. The anodization current density waveform profile follows equation 4.1. A pore widening treatment was performed after anodization in order to widen the nanopore diameter in each NAA-MPSs and study the influence of the porosity on their optical properties by wet chemical etching in H<sub>3</sub>PO<sub>4</sub> 5% wt at 35°C. The pore widening treatment was applied for different times, from 0 to 25 min, in an interval of 5 min.

**Table 4.1**. Summary of fabrication conditions and period thickness of samples NAA-MPSs-A, B, C, and D.

Sample	$J_0$	$J_1$	T <sub>1</sub>	T <sub>2</sub>	T <sub>3</sub>		Period	d Thickness [nm]	
	[mAcm <sup>2</sup> ]	[mAcm <sup>2</sup> ]	[s]	[s]	[s]	N	Layer 1	Layer 2	Layer 3
A	2.6	1.3	150	175	200	1	180	210	240
В	2.6	1.3	160	175	190	1	192	210	228
С	2.6	1.3	165	175	185	1	198	210	222
D	2.6	1.3	170	175	180	1	204	210	216

## 4.2.2 Optical Characterization of Multi-Spectral Photonic Structures

The reflection spectra of multi-spectral NAA-MPSs across the UV-visible-NIR spectrum were measured at 8º of incidence angle with a resolution of 2 nm in a Perkin Elmer UV-Visible-NIR Lambda 950 spectrophotometer. The effective medium of these NAA-PCs was assessed in real-time by quantifying spectral shifts in the positions of the characteristics photonic stopbands of NAA-MPSs upon infiltration with D-glucose solutions of different refractive index. This process was performed in real-time in a

flow cell made of acrylic plastic. Reflectance spectra of multi-spectral NAA-MPSs were obtained using a halogen light source and a spectrometer. Light was directed onto the surface of NAA-MPSs at normal angle through a bifurcated fiber optic cable consisting of six illuminating waveguides and one reading waveguide coupled to an optical lens that focused the light on the top of the NAA-MPSs. The light reflected was collected by the spectrometer, which recorded one spectrum every 2 s. Reflectance spectra were acquired for the wavelength range 400-800 nm.

The sensitivity of the effective medium of the NAA-MPSs was assessed by infiltrating their nanoporous structure with glucose solutions at different concentrations (0.025, 0.05, 0.125, 0.250, 0.50, 0.75, and 1M). Upon the infiltration, the characteristic forbidden bands undergo spectral shifts due to changes in the refractive index of the medium filling the nanopores. These changes are quantified in real time using deionized water (DI) as a baseline at constant rate of 500  $\mu$ l min<sup>-1</sup>, between each infiltration a washing step with (DI).

The interferometric color of multi-spectral NAA-MPSs was characterized by digital pictures, acquired by a Canon EOS 700D digital camera equipped with Tamron 90 mm F2.8 VC USD macro mount lens with autofocus function under natural light illumination.

#### 4.2.3 Structural Characterization of NAA-MPSs

The structural characterization of multi-spectral NAA-MPSs was performed using an environmental scanning electron microscope (ESEM FEI Quanta 600) operating at an accelerating voltage between 20 and 25 keV. ESEM images were analyzed by ImageJ software.

### 4.2.4 Modelling of NAA-MPSs

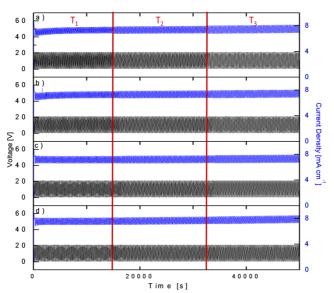
The optical properties of multi-spectral NAA-MPSs were modelled using an effective medium approximation (EMA) and the transfer matrix method (TMM). The effective refractive index of each layer in the structure of NAA-MPSs was calculated using the Looyenga-Landau-Lifshitz (3L) formula in combination with that reported from Bartzsch et al. 54,55 Calculation of the reflectance spectra was performed by means of the transfer matrix method using MatLab® software.

### 4.3 Results and Discussion

#### 4.3.1 Fabrication and structural Characterization of NAA-MPSs

**Figure 4.2** shows a representative anodization current density profile for each T<sub>i</sub> applied during the fabrication of multi-spectral NAA-MPSs and the measured voltage response of the system. This graph reveals that the anodization voltage (output) follows the sinusoidal variations of the applied anodization current density (input) with a certain delay.

Anodization is an electrochemical process that relies on the flow of the electronic and ionic species across the oxide barrier layer located at the nanopores' bottom. Dynamic modifications of the anodizing current density alter the steady flow of electronic and ionic species across the oxide barrier layer, which needs a recovery time to achieve its equilibrium state again. This time delay depends on the thickness of the oxide barrier layer and the level of anodizing current density change<sup>20,56,57</sup>.

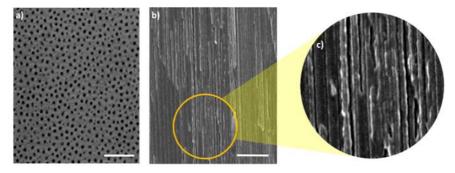


**Figure 4.2**. Evolution of the anodization current density and voltage during the fabrication of NAA-MPSs. (a) Anodization voltage and current density profile of sample NAA-MPSs-A  $J_0=2.6~\text{mAcm}^{-2}$ ,  $J_1=1.3~\text{mAcm}^{-2}$ ,  $T_1=150$ ,  $T_2=175$  and  $T_3=200~\text{s}$  and  $T_3=100~\text{periods}$ . (b) NAA-MPSs-B  $J_0=2.6~\text{mAcm}^{-2}$ ,  $J_1=1.3~\text{mAcm}^{-2}$ ,  $T_1=160$ ,  $T_2=175~\text{and}$   $T_3=190~\text{s}$  and  $T_3=180~\text{s}$  and  $T_3=185~\text{s}$  and  $T_3=185~\text{s}$  and  $T_3=185~\text{s}$  and  $T_3=185~\text{s}$  and  $T_3=180~\text{s}$  and  $T_3=18$ 

It is remarkable that the amplitude of the measured voltage increases with the anodization period (i.e.,  $T_1$ ,  $T_2$  and  $T_3$ ) despite of keeping constant the rest of the parameters ( $J_0$  and  $J_1$ ). From this analysis, it is inferred that the porous layer growth has a dynamic behavior governed by a characteristic reaction time established by the anodization period. The anodization current density sinusoidal waves featuring three sequentially increasing anodization periods are translated into the material's structure as stacked PCs based on NAA-MPSs in the same structure.

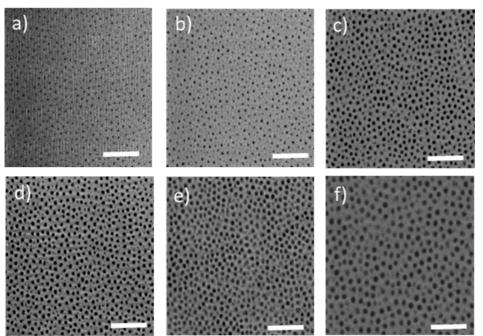
For each NAA-PC embedded within the structure of the multi-spectral NAA-MPS, the pore diameter varies sinusoidally in depth. The optical response of the composite NAA-MPSs presents several forbidden bands, one for each NAA-MPS composing the overall PC structure. **Figure 4.3** 

shows representative ESEM images of a representative multi-spectral NAA-MPS produced in this study. The top view image shows nanopores randomly distributed across the surface of the PC structure (Figure 4.3a) the pore average of this sample (NAA-MPSs-A) is ~45 nm due to the pore widening treatment of 10 minutes. The general cross section of the samples shown in Figure 4.3b reveals the oscillating pattern in depth of the pore diameter. Figure 4.3c shows a magnified view of the yellow circle in figure 4.3b. The pore morphology of the NAA-MPSs induces a modification in depth of the porosity, which results in a sinusoidal variation of the effective refractive index in depth.



**Figure 4.3**. Structural characterization of a NAA-MPSs- produced with offset density current  $J_0=2.6$  mAcm<sup>-2</sup>, amplitude density current  $J_1=1.3$  mAcm<sup>-2</sup>, N=100 periods,  $T_1=150$ ,  $T_2=175$ ,  $T_3=200$  s and pore widening time of 10 min (a) ESEM top view (scale bar: 1  $\mu$ m). (b) ESEM General cross section (scale bar: 2  $\mu$ m). (c) Magnified view of yellow circle of NAA-MPSs.

An EMA (effective medium approximation) model was employed to design the NAA-MPSs structure as a multilayer system and provide a mechanistic explanation of the optical properties of multi-spectral NAA-MPSs. The pore diameter can be precisely controlled by the pore widening time from 0, 5, 10, 15, 20 and 25 min, which correspond to pore diameters of 35, 40, 45, 50, 55 and 60 nm, respectively (Figure 4.4).

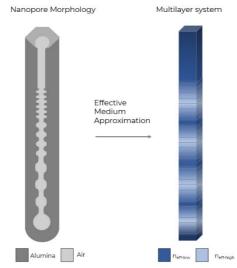


**Figure 4.4.** Structural characterization of a NAA-MPSs- produced with offset density current  $J_0=2.6$  mAcm<sup>-2</sup>, amplitude density current  $J_1=1.3$  mAcm<sup>-2</sup>, N=100 periods,  $T_1=170$ ,  $T_2=175$ ,  $T_3=180$  s (a) ESEM top view of sample with  $t_{pw}=0$  min (pore diameter= 35 nm) (scale bar: 1  $\mu$ m). (b) sample with  $t_{pw}=5$  min (pore diameter= 40 nm), (c) sample with  $t_{pw}=10$  min (pore diameter= 45 nm), (d) sample with  $t_{pw}=15$  min (pore diameter= 50 nm), (e) sample with  $t_{pw}=20$  min (pore diameter= 55 nm), (f) sample with  $t_{pw}=25$  min (pore diameter= 60 nm).

**Figure 4.5** shows an illustration of the transition of the NAA-MPSs pore morphology into an effective graded-index model that follows the pore growth direction. This system is composed of multiple layers with constant refractive index which oscillates between a high refractive index and a low refractive index value along the nanopore's length. NAA-MPSs fabricated in this study present three different forbidden bands, the spectral position of which is established by the anodization period  $T_i$  (i=1,2,3). The central anodization period  $T_2$  is kept constant ( $T_2$ = 175 s), which means that the position of the central band is approximately the same for all the NAA-MPSs. However, the values of the other two periods

(T<sub>1</sub> and T<sub>3</sub> were systematically modified in each NAA-MPSs in order to demonstrate the tuneability of the bands separation and its effect on the sensitivity of these composite PCs.

As summarized in **Table 4.1**, NAA-MPSs-A were produced with  $T_1$ = 150,  $T_2$ = 175 and  $T_3$ = 200 s, NAA-MPSs-B were fabricated with  $T_1$ = 160,  $T_2$ = 175 and  $T_3$ = 190 s, NAA-MPSs-C with  $T_1$ = 165,  $T_2$ = 175 and  $T_3$ = 185 s, and NAA-MPSs-D with  $T_1$ = 170,  $T_2$ = 175 and  $T_3$ =180 s.



**Figure 4.5.** Transition of the NAA-MPS nanopore morphology towards a multilayered system in which the constant effective refractive index of each layer varies between n<sub>eff-low</sub> and n<sub>eff-high</sub>.

### 4.3.2 Optical characterization and modelling of NAA-MPSs

All the studied multi-spectral NAA-MPSs were fabricated with  $J_0$ =2.6 mAcm<sup>-2</sup>,  $J_1$ = 1.3 mAcm<sup>-2</sup> with constant number of periods (N = 100 periods) whereas the values of the three periods  $T_i$  vary from one to the other. Figure 5a shows the reflectance spectra of multi-spectral NAA-MPSs with varying  $T_i$ . Three forbidden bands can be clearly observed for all these

NAA-MPSs, which show a narrow width, with an average of full width and half maximum (FWHM) between 12 to 20 nm. It can be observed that the central forbidden band is positioned at the same wavelength for all the multi-spectral NAA-MPSs since all of them were fabricated with the same  $T_2$  (175 s).

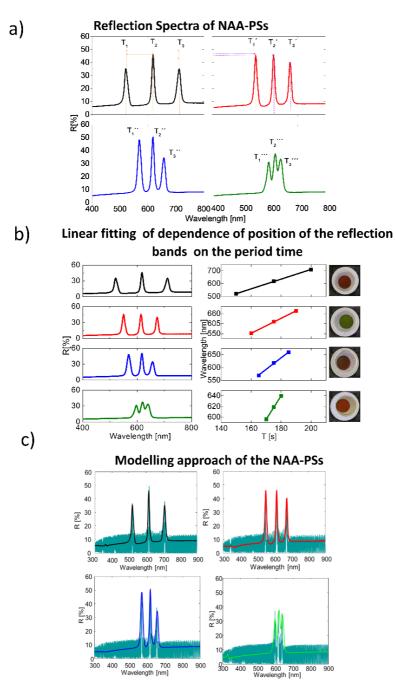
On the contrary,  $T_1$  and  $T_3$  were systematically modified to demonstrate the tuneability of this class of PC system across the visible spectrum. The position of the forbidden bands depends on the anodization period, which can be precisely tuned by increasing or decreasing  $T_1$  and  $T_3$  (i.e., red shift —move towards longer wavelengths or blue shift move towards shorter wavelengths).

**Figure 4.6a** shows the position of the forbidden bands for four different combinations of anodization periods. The excellent repeatability and controllability of the anodization system is observed in this graph as all the NAA-MPSs- present a central forbidden band at  $618 \pm 1$  nm, which is associated with the NAA-MPS produced with  $T_2$ = 175 s. For the NAA-MPSs-A, the position of the reflection bands for  $T_1$  = 150 s,  $T_2$  = 175 s,  $T_3$  = 200 s were located at in the 520, 618 and 712 nm, respectively. In the case of NAA-MPSs-B, the forbidden bands were located in 553, 616 and 673 nm, which correspond to  $T_1$ =160 s,  $T_2$  = 175 s and  $T_3$  = 190 s, respectively. The position of the forbidden bands of NAA-MPSs-C produced with  $T_1$ = 165 s  $T_2$ = 175 s and  $T_3$ = 185 s were in 570, 618 and 660 nm, respectively. Finally, the reflection bands of NAA-MPSs-D were located in 596, 619 and 640 nm, which correspond to the embedded NAA-MPSs fabricated with  $T_1$ = 170 s,  $T_2$ = 175 s and  $T_3$ = 180 s.

Figure 4.6b shows that the position of the three forbidden bands have a linear dependence with the corresponding anodization period ( $T_1$ ,  $T_2$  and  $T_3$ ). These linear fitting make it possible to design the spectral fingerprint of each multi-spectral NAA-MPS (i.e. position of the forbidden bands) across the entire spectrum to fulfil the requirement of different applications. Digital images of these multi-spectral NAA-MPSs reveal that these PCs display vivid interferometric color, which is established by the position of the characteristic reflection bands.

For the samples NAA-MPSs-A, C and D the interferometric color is red while the sample NAA-MPSs-B is green. The interferometric color exhibit by these photonics structures is established by the band located at longer wavelengths 712, 660 and 640 nm for samples NAA.GIFs-A, C, and D respectively and in the case of sample B the interferometric color is given by the closer wavelength 553 nm.

**Figure 4.6c** shows a compilation of experimental and simulated reflection spectra for the multi-spectral NAA-MPSs fabricated in this study. The simulation results show that the three reflection bands of the multi-spectral NAA-MPS (cyan lines) are in good agreement with the experimental reflection spectra of the samples. These graphs show that the transfer matrix model developed in this study can precisely predict the spectral fingerprint of these complex PCs. This model provides a mechanistic explanation of the light–matter interactions occurring within these PCs, opening new opportunities to design novel PC architectures for specific applications.



**Figure 4.6.** Reflection spectra of NAA-MPSs of samples A-D (Described in table 1). (a) Reflection spectra of all samples (NAA-MPS-A-D). (b) Position of the reflection bands of NAA-MPSs in (a-d) as a function of period time (T). The linear regression is plotted for each NAA-MPSs. Digital pictures of NAA-MPSs A-D (c) Modelling approach of all the samples (NAA-MPSs-A-D) cyan lines represent the modelling approximation of the NAA-MPSs spectra and the black, red, blue and green represent de experimental spectra of samples.

## 4.3.3 Pore Widening Effect in the Optical Properties of Multi-Spectral NAA-MPSs.

To study the effect of the pore widening time on the optical properties of multi-spectral NAA-MPSs, the reflectance spectrum of these NAA-MPSs fabricated with  $J_0$ = 2.6 mAcm<sup>-2</sup>,  $J_1$ = 1.3 mAcm<sup>-2</sup> and  $T_1$ = 165,  $T_2$  =170 and  $T_3$ =175 s was measured at different pore widening times ( $t_{pw}$ ): 5, 10, 15, 20 and 25 min, which correspond to nanopore diameters of 35, 40, 45, 50, 55 and 60 nm, respectively (**Figure 4.7**).

**Figure 4.7a** shows the reflection spectra with  $t_{pw}$ . At  $t_{pw}=0$  (i.e., asproduced NAA-MPSs, average of pore diameter ~35 nm) the position of the reflection bands was located at 578, 606 and 628 nm for  $T_1$ = 165 s,  $T_2$ = 170 s and  $T_3$ = 175 s, respectively. The reflection bands present a maximum reflection intensity of 32.3, 51.8 and 57.8 %, respectively, and a FWHM of 24, 18 and 16 nm. At  $t_{pw}$ = 5 min (i.e., pore diameter ~ 40nm), the reflection bands are blue-shifted to 568, 598 and 622 nm, the maximum reflection for these bands were 34.8, 55.2, 60.3 % and their FWHM were 31, 18 and 18 nm, respectively. In the case of  $t_{pw}$  = 10 min (i.e., average of pore diameter of 45 nm), the position of the forbidden bands was located at 558, 592 and 618 nm, the maximum reflection for these bands were 46.0, 54.8 and 46.5 %, and the FWHM were 32, 20 and 20 nm, respectively.

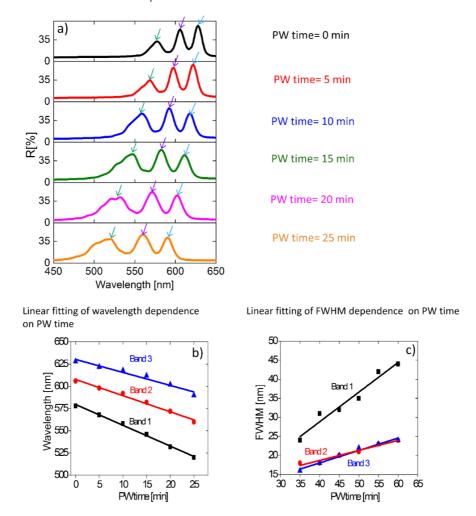
For  $t_{pw}$  = 15 min (average of pore diameter ~50 nm), the position of the forbidden bands was 546, 582 and 612 nm, the maximum reflection for these bands were 45.4, 52.8, and 43.8 %, and the FWHM of the bands were 35, 21 and 22 nm respectively. The position of the reflection bands for  $t_{pw}$  = 20 min (i.e., pore diameter ~55 nm) were 532, 572 and 602 nm,

with a maximum reflection of 42.2, 49.7 and 44.3 % and FWHM of 42, 23 and 23 nm, respectively. At  $t_{pw}$ = 25 min (average pore diameter of 60 nm), the position of the forbidden bands was situated at 520, 560 and 590 nm, the maximum reflection of the bands were 38.8, 46.1 and 41.3 % and the FWHM for these forbidden bands were 44, 24 and 24 nm, respectively.

**Figure 4.7b** shows the linearity between  $t_{pw}$  and the position of the three forbidden bands. This graph indicates that the position of the forbidden bands blue shifts linearly when tpw increases from 0 to 25 min. However, the blue shift rate (i.e., slope of linear fitting) depends on the position of the forbidden band: the slope of band 1 is greater than that of bands 2 and 3. The slopes of the fitting lines for the three forbidden bands of multispectral NAA-MPSs produced were found to be -2.34 ( $T_1$ = 165 s), -1.46 ( $T_2$  = 170 s) and -1.81 ( $T_3$  = 175 s) nm min<sup>-1</sup>.

The relation between the  $t_{pw}$  and the FWHM is presented in **Figure 4.7c**. For band 1, we can observe that a high increment of the FWHM with  $t_{pw}$ , whereas for bands 2 and 3 the increment is less marked. For the three bands, the increment of FWHM depends linearly on the pore widening time. The slopes of the fitting lines for the FWHM of the three forbidden bands of multi-spectral NAA-MPSs produced with  $T_1 = 165$  s,  $T_2 = 170$  s and  $T_3 = 175$  s, were found to be 0.78, 0.32 and 0.26 nm min<sup>-1</sup>, respectively. The difference observed between band 1 and the rest of bands can be explained by observing the NAA structure of the multi-spectral NAA-MPSs. The three bands of these NAA-PCs are generated by three different NAA-MPSs stacked one over another.





**Figure 4.7.** (a) Effect of the pore widening on the reflection spectrum of a NAA-MPSs with  $J_0$ = 2.6 mAcm<sup>-2</sup>,  $J_1$ = 1.3 mAcm<sup>-2</sup> and  $T_1$ = 165,  $T_2$ = 170 and  $T_3$ = 175 s was measured for different pore widening times: 0, 5, 10, 15, 20 and 25 min. (b) linear fitting lines showing the dependence between the position of the reflection bands and pore widening time (c) Linear fitting showing the dependence between Full width at half maximum (FWHM) and pore widening time.

**Table 4.2** summarizes the effect of the six different  $t_{pw}$  on the position of the forbidden bands, their intensity, and their FWHM. The position of the characteristic forbidden bands undergoes a blue shift when the PC structure is etched and the size of its nanopores is widened. The NAA-MPS that generates band 1 is at the top of the composite multi-spectral NAA-

MPSs structure. Chemical etching at the top part of the composite NAA-MPS is more effective than within the nanoporous structure due to limited diffusion of chemical species. Therefore, the top NAA-MPS structure is etched at a slightly faster rate than its counterparts located at lower positions within the composite NAA-MPS. This results in a differential etching rate that leads to distinct blue shifts in the position of the characteristic forbidden bands of the multi-spectral NAA-MPSs. Whereas the other two NAA-MPSs, generating bands 2 and 3, are underneath and their complete NAA structure is affected by the etching dissolution in a similar way.

**Table 4.2**. Summary of the effect of the pore widening on the reflectance spectrum of NAA-MPSs.

Pore widening time	Average Pore	Band	$\lambda_{band}$	R <sub>max</sub>	FWHM	
(min)	diameter (nm)		(nm)	(%)	(nm)	
		1	578	32.3	24	
0	35	2	606	51.8	18	
		3	628	57.8	16	
		1	568	34.8	31	
5	40	2	598	55.2	18	
		3	622	60.3	18	
		1	558	46.0	32	
10	45	2	592	54.8	20	
		3	618	46.5	20	
		1	546	45.4	35	
15	50	2	582	52.8	21	
		3	612	43.8	22	
		1	532	41.2	42	
20	55	2	572	49.7	23	
		3	602	44.3	23	
		1	520	38.8	44	
25	60	2	560	46.1	24	
		3	590	41.3	24	

The average pore diameter also affects the amplitude of the forbidden band and it's FWHM (Table 4.2). When increasing the average pore diameter from 35 to 60 nm, the FWHM of band 1 increases from 24 to 44 nm, for band 2 increases from 18 to 24 nm and for band 3 from 16 to 24 nm. The maximum reflectance of the bands increases with the pore diameter until 50 nm, after which the reflectance intensity decreases.

Therefore, two different response regions can be differentiated: the pore diameter increases the maximum reflectance of the forbidden band until 50 nm and decreases beyond this pore size. This phenomenon can be associated with diffusive light scattering by the overall PC structure due to increased porosity.

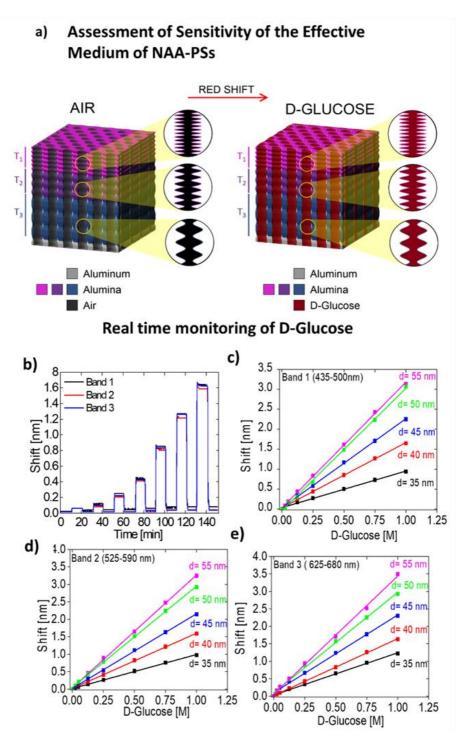
# 4.3.4 Assessment of the Sensitivity of the Effective Medium of NAA-MPSs

To study the potential use of multi-spectral NAA-MPSs structures as sensing platforms, we assessed in real-time the spectral shifts in the three characteristic forbidden bands of these NAA-MPSs by filling the pores with analytical solutions D-glucose with different concentrations. The variation of the effective refractive index of the medium filling the nanopores of multi-spectral NAA-MPSs red-shifts the position of the characteristic forbidden bands. These experiments were performed for different pore diameters in order to study the sensitivity of the PC structure when the pore diameter is increased. To this end, first a base line was obtained using deionized water, which was injected into the flow cell for 10 min until a stable base line was achieved. Then, analytical solutions of D-glucose 0.025 - 1.0 M were flowed at a constant rate of  $500 \mu L \text{ min}^{-1}$ .

A cleaning step flowing fresh deionized water was carried out between each analytical solution of D-glucose in order to clean the remaining glucose molecules within the pores. **Figure 4.8** shows the assessment of sensitivity of the effective medium of multi-spectral NAA-MPSs. We can observe that the shift of the forbidden band positions increases when the D-glucose concentration increases, which indicates the utility of these PCs for sensing applications.

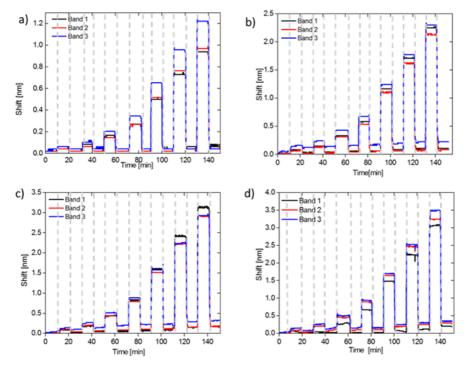
**Figure 4.8a** shows a scheme of the infiltration of multi-spectral NAA-MPSs nanopores with different concentration of D-glucose. This infiltration produces a red shift (shift toward higher wavelengths) in the position of the forbidden bands. **Figure 4.8b** shows the real-time measurements of a multi-spectral NAA-MPS with pore diameter of 40 nm ( $t_{pw} = 5$  min). **Figures 4.8c-e** show the linear dependence between the shift of the forbidden bands and the concentration D-glucose for each pore diameter and band structure.

**Figure 4.8c** shows the fitting lines for band 1 with reflection bands situated between 435 and 500 nm, which correspond to each pore widening time. The sensitivity (S) for each pore diameter in band 1 was 0.91 (35 nm), 1.64 (40 nm), 2.23 (45 nm), 3.15 (50 nm) and 3.07 (55 nm) nm M<sup>-1</sup> and with a limit of detection of (LOD) 6.8, 1.3, 5.2, 3.5 and 5.5 mM, respectively. **Figure 4.8d** shows the results for band 2 (525-590 nm), the sensitivity (S) for each pore diameter of band 2 were 0.97 (35 nm), 1.64 (40 nm), 2.13 (45 nm), 2.90 (50 nm) and 3.23 (55 nm) nm M<sup>-1</sup>, with a limit of detection of (LOD) 2.2, 1.9, 5.3, 3.7 and 2.8 mM, respectively.



**Figure 4.8.** (a) Assessment of the effective medium assessment of NAA- GIFs. (b) Real time monitoring of D-Glucose concentrations 0.025, 0.05, 0.125, 0.25, 0.5, 0.75 and 1.0 M for 40 nm of pore diameter. Sensitivity approach for different pore diameters (35, 40, 45, 50 and 55 nm) for (c) band 1, (d) band 2, and (e) band 3.

**Figure 4.8e** summarizes the results for the band 3 (625-680 nm). The sensitivity (S) of each pore diameter of band 3 were 1.21 (35 nm), 1.63 (40 nm), 2.22 (45 nm), 2.87 (50 nm) and 3.38 (55 nm) nm M<sup>-1</sup>, with a limit of detection of (LOD) 1.7, 1.8, 6.4, 3.7 and 1.7 mM, respectively. The results of the average of pore diameters of 35 (t<sub>pw</sub>=0 min), 45(t<sub>pw</sub>=10 min), 50 (t<sub>pw</sub>=15 min) and 55 (t<sub>pw</sub>=20 min) nm are shown in **Figure 4.9.** The infiltration of each analytical solution of D-glucose produces a redshift in the position of the bands. However, this change was reversible due to the lack of a chemical interaction between glucose molecules and the NAA-MPSs surface. **Table 4.3** summarizes the sensitivity and LOD characteristics of the multi-spectral NAA-MPSs obtained from the effective medium assessment.

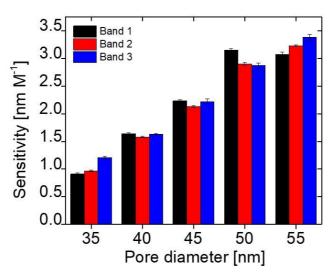


**Figure 4.9**. Real time monitoring of D-Glucose concentrations 0.025, 0.05, 0.125, 0.25, 0.5, 0.75 and 1M. (a) Pore diameter = 35 nm ( $_{tpw}$ = 0min), (b) Pore diameter = 45 nm ( $_{tpw}$ = 10min), (c) Pore diameter = 50 nm ( $_{tpw}$ = 15min) and (d) Pore diameter = 55 nm ( $_{tpw}$ = 20 min).

**Table 4.3.** Sensitivity and limit of detection (LOD) of NAA-MPSs in the real time monitoring experiments.

Average Pore	Band	S [nm M <sup>-1</sup> ]	LOD [mM]
D = 35 nm	1	0.91	6.8
(t <sub>pw</sub> = 0min)	2	0.97	2.2
(tpw – Ollilli)	3	1.21	1.7
D = 40 nm	1	1.64	1.3
	2	1.58	1.9
(tpw = 5 min)	3	1.63	1.8
D = 45 nm	1	2.23	5.2
(tpw= 10 min)	2	2.13	5.3
(tpw=10 mm)	3	2.22	6.4
D = 50 nm	1	3.15	3.5
(tpw= 15 min)	2	2.90	3.7
(tpw- 15 iiiii)	3	2.87	3.7
D = 55 nm	1	3.07	5.5
(tpw= 20 min)	2	3.23	2.8
(CPW- 20 IIIII)	3	3.38	1.7

Figure 4.10 provides a bar chart comparing the sensitivity of the different PC structures. From these results, we can conclude that when the pore diameter in the structure of multi-spectral NAA-MPSs is increased, the shift of the forbidden band position increases linearly in all the cases, being more than three times greater for 55 nm than for 35 nm. Also, it is worthwhile noting that band 3 is in general more sensitive to effective refractive index variations than bands 1 and 2.



**Figure 4.10**. Sensitivity of each forbidden band of the NAA-MPSs for the different pore diameters (35, 40, 45, 50 and 55 nm) for the three bands.

### 4.4 Conclusion

In this chapter, we fabricated stacked photonic crystals based on nanoporous anodic alumina gradient-index filters (NAA-MPSs) with complex optical response by the application of successive sinusoidal anodization current density profiles. The position of the forbidden bands presented by these multi-spectral NAA-MPSs can be accurately tuned by varying the anodization period of the anodization current density waveform. Furthermore, we assess the effect of the porosity of the structure on the reflection spectrum by applying a pore widening chemical etching treatment from 0 to 25 min. The increment of the pore diameter blue-shifts the position of the forbidden bands. A lineal relation between the increments of the pore widening times and the position of the forbidden bands can be observed. The intensity and width of the bands also increases with the pore widening.

We also demonstrated the ability of multi-spectral NAA-MPSs structures for sensing applications by detecting small changes of the effective refractive index due to the fluid filling of the pores. Different concentrations of D-glucose have been successfully detected and quantified in real-time. These real-time experiments, carried out by increasing the average pore diameter from 35 nm to 55 nm, indicate that the sensitivity is different for each forbidden band and it depends on the pore diameter of the multi-spectral NAA-MPS structure: the increment of the pore diameter leads to an enhancement in sensitivity of the photonic crystal structure.

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UNIVERSITAT ROVIRA I VIRGILI

ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla

# Chapter 5. Nanoporous Anodic Alumina Photonic Structures by Gaussian Pulse Anodization

UNIVERSITAT ROVIRA I VIRGILI ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla This Chapter presents a Gaussian pulse anodization approach to generate nanoporous photonic crystals with highly tunable and controllable optical properties across the visible—NIR spectrum. Nanoporous anodic alumina Gaussian photonic crystals (NAA-GPSs) are fabricated in oxalic acid electrolyte by Gaussian pulse anodization —a novel form of pulse-like anodization. The effect of the Gaussian pulse width in the anodization profile on the optical properties of these photonic crystals is assessed by systematically varying this fabrication parameter from 5 to 60 s. The effective medium of NAA-GPSs is assessed by monitoring spectral shifts in their characteristic PSB upon infiltration of their nanoporous structure with analytical solutions of D-glucose of varying concentration

#### 5.1 Introduction

Photonic structures (PSs) are dielectric optical forms with specifically engineered photonic bands to modify the group velocity of photons when these flow through the PC. Light–matter interactions in PCs can be tuned with precision by engineering the PC's architecture so regions with high and low refractive index are periodically and spatially distributed <sup>1-8</sup>. Distinct forms of PCs based on a wide range of materials can be produced to harness versatile control over electromagnetic waves across the broad spectrum, from UV to IR. PCs have found multiple applications, including photonic encoding<sup>9</sup>, chemical sensing and biosensing<sup>10-14</sup>, lasing<sup>8</sup>, and photocatalysis<sup>15,16</sup>. Since the pioneering works by Masuda and coworkers, nanoporous anodic alumina (NAA) is an ideal base material to generate nanoporous PCs<sup>17-19</sup> due to its cylindrical nanopores with well-defined and highly controllable geometric features. NAA is produced by anodization of aluminum films, which is a cost-effective and fully scalable

top-down industrial process compatible with traditional micro- and nanofabrication<sup>20-22</sup>. The optical properties of NAA are intrinsically dependent on the architecture, dimensions and distribution of its nanopores, which can be precisely engineered during the anodization process. Therefore, structural engineering of NAA enables new paths to modulate its effective refractive index in 1D, 2D or 3D distributions to form PC structures such as distributed Bragg reflectors<sup>23-26</sup>, microcavities<sup>27</sup>, and gradient index filters<sup>15,16,28-30</sup>. NAA-PC structures have demonstrated unique optical properties to guide, reflect, transmit, emit, and enhance incident photons for specific applications. Recent progress in anodization technology has focused on structural engineering of NAA-PCs by distinct forms of pulse-like anodization approaches such as sinusoidal<sup>14,28,29-33</sup>, sawtooth<sup>34</sup>, pseudostepwise<sup>35</sup>, and stepwise<sup>27</sup>.

In contrast to pioneering pulse-like anodization combining hybrid pulses between mild and hard anodization regimes<sup>37-40</sup>, pulse anodization performed under mild conditions<sup>41</sup> moderate electrolyte temperature and anodizing voltage/current density— provide superior controllability over the anodic oxide growth rate and its porosity, enabling new paths to engineering the structure of NAA with precision to achieve versatile control of light for specific applications such as optical sensing <sup>42,43</sup>, and biosensing<sup>22,44-47</sup> and photocatalysis<sup>15</sup>. Despite these advances, to date only a limited number of pulse shapes have been implemented into anodization approaches to engineering distinct forms of NAA-based PCs, including sinusoidal, symmetric and asymmetric stepwise, and sawtooth. Although these strategies have successfully realized the engineering of NAA-PCs with outstanding optical properties, further developments of

anodization technology will be needed to tailor-engineer the structure of NAA–PCs with versatility for harnessing specific forms of light–matter interactions and spreading the applicability of these unique PC structures across light-based technologies. Motivated by these efforts, herein we present an innovative pulse-like anodization approach that makes it possible to engineer a novel form of NAA-PCs using Gaussian current density pulses.

The position of central wavelength, full width at half maximum and intensity of the characteristic photonic stopband (PSB) of NAA-PCs in their reflection spectrum are demonstrated to rely strongly on the Gaussian pulse width, the incidence angle of light and the porosity of NAA-PCs. We also demonstrate that Gaussian NAA-PCs (NAA-GPSs) produced by Gaussian pulse anodization are highly sensitive to alterations in their effective medium, showing promising potential to be integrated as platform materials for optical sensing and biosensing systems. The findings establish a rationale to better understand the effect of key anodization parameters on the optical properties of NAA-GPSs, providing exciting opportunities to engineer NAA-PCs with finely tuned optical properties for specific light-based technologies.

#### 5.2 Fabrication Details

## **5.2.1** Fabrication of NAA-GPSs by Gaussian Pulse Anodization

Impurities and grease in as-received aluminum substrates were removed by thoroughly sequential washing in acetone, ethanol, and water. Prior to anodization, aluminum substrates were electropolished in an electrolyte 4:1 v/v ethanol–perchloric acid at 20 V and 5°C for 6 min, with the stirring

direction alternated from clockwise to anticlockwise every 60 s. Electropolished aluminum discs were then anodized in 0.3 M aqueous oxalic acid electrolyte at 5°C using a current density—time anodization profile featuring Gaussian pulses generated according to Equation 1, for a number of pulses *N*:

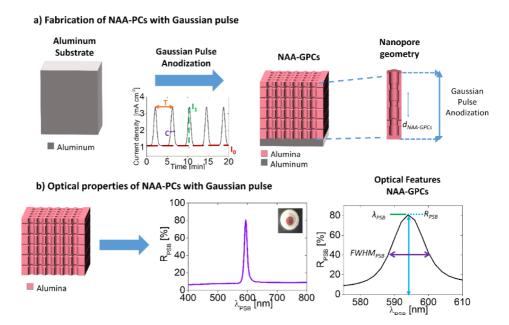
$$J(t) = J_0 + J_1 exp^{\frac{-[t - \frac{T}{2}]^2}{2c^2}}$$
 (5.1)

where J(t) is the anodization current density at time t,  $J_1$  is the current density amplitude, T is the anodization period,  $J_0$  is the offset current density and C is the width of the Gaussian pulse. **Figure 5.1a** illustrates the fabrication process used to generate NAA-GPSs via gaussian pulse anodization, including a representative anodization profile with a graphical description of the fabrication parameters (current density offset  $-J_0=1.13$  mA cm<sup>-2</sup>, current density amplitude  $-J_1=2.26$  mA cm<sup>-2</sup>, anodization period -T=250 s, number of pulses- N=150 periods and Gaussian pulse width -C=20 s), and the schematic description of the most representative structural features defining the structure of NAA-GPSs (i.e., pore length  $-L_{NAA-GPSs}$  and period length  $-d_{NAA-GPSs}$ ).

**Figure 5.1b** shows interlink between the nanoporous structure and the optical properties of NAA-GPSs, with a representative reflection spectrum of a NAA-GPS produced with  $J_0 = 1.13$  mA cm<sup>-2</sup>,  $J_1 = 2.26$  mA cm<sup>-2</sup>, T = 250 s, N = 150 pulses and C = 20 s. Notice that, the inset shows a digital picture acquire with dark background of that NAA–GPS displaying vivid redorange interferometric color) (center), and magnified view of the photonic stopband (PSB) of that NAA-GPS with a graphical description of its optical

features (i.e., reflection intensity –  $R_{PSB}$ , central wavelength –  $\lambda_{PSB}$  and full width and half maximum –  $FWHM_{PSB}$ ) (right).

For optical characterization purposes, after anodization the remaining aluminum substrate was chemically etched from the backside of NAA-GPSs by selective chemical etching in a saturated  $HCl-CuCl_2$  solution for optical characterization. To study the effect of porosity on the optical properties of NAA-GPSs, the nanopores of these PCs were widened after anodization via wet chemical etching in an aqueous solution of  $H_3PO_4$  5 wt% at 35°C and varying time, from 0 to 20 min, with a time interval of 5 min.



**Figure 5.1.** Fabrication of nanoporous anodic alumina Gaussian photonic structures (NAA-GPSs) using Gaussian pulse anodization. (a) Representative Gaussian pulse anodization profile used to produce NAA-GPSs. (b) Schematics showing relationship between structure (left), optical reflection spectrum of a representative NAA-GPS produced.

# **5.2.2 Optical Characterization of NAA-GPSs Produced by Gaussian**Pulse Anodization

Reflection spectra of NAA-GPSs were measured from 250 to 900 nm with a resolution of 2 nm at varying incidence angle from 8 to 60° in a PerkinElmer UV-visible–NIR Lambda 950 spectrophotometer. The reflection intensity ( $R_{PSB}$ ), quality factor ( $Q_{PSB}$ ) and full width at half maximum ( $FWHM_{PSB}$ ) of the PSB of NAA-GPSs were estimated from the reflection spectra, using Gaussian fittings. The effective medium of NAA-GPSs was assessed by measuring spectral shifts in the position of their PSB upon infiltration with analytical solutions of D-glucose with varying refractive index. This process was performed under continuous fluidic flow conditions at a fixed rate of 500  $\mu$ L min<sup>-1</sup> in real-time using an acrylic plastic-based flow cell. Reflectance spectra from NAA-GPSs were acquired using a setup combining a halogen light source (Spectligth DH-c) and an optical fiber spectrometer (Avantes, AvaSpec-3648).

Light from the source was focused onto the surface of NAA-GPSs at normal incidence using a bifurcated fiber optic probe with six illuminating waveguides assembled around one central reading waveguide. The Optical probe was coupled to an optical lens to focus light within a ~1 mm-diameter circular spot on the top of NAA-GPSs. Collection of reflected light was performed by the optical fiber probe and guided to the spectrometer, which recorded one spectrum every 2 s with and integration time of 50 ms. Reflectance spectra were measured for the wavelength range of 400–900 nm. The resulting data were processed by a custom-made program in MATLAB software.

# 5.2.3 Structural Characterization of NAA-GPSs Produced by Gaussian Pulse Anodization

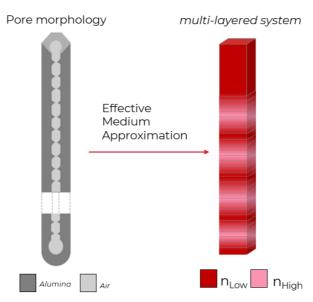
The structure of Gaussian NAA-GPSs was characterized by a field-emission gun scanning electron microscopy (FEG-SEM FEI Quanta 450) and an environmental scanning electron microscopy (ESEM FEI Quanta 600) operating at an accelerating voltage between 20 and 25 keV. ESEM and FEG-SEM images were analyzed by ImageJ <sup>48</sup>.

## **5.2.4 Modeling of Gaussian NAA-GPSs**

The optical properties of Gaussian NAA-GPSs were modeled by combining an effective medium approximation (EMA) model and the transfer matrix method (TMM). The effective refractive index of each layer within NAA-GPSs' structure was estimated by the Looyenga–Landau–Lifshitz (3L) EMA model in combination with that reported from Bartzsch<sup>31,49</sup> and Kuang<sup>50</sup>.

Figure 5.2 shows an illustration of the discretization of effective refractive index in NAA-GPSs as a 1D-effective graded-index system in the pore growth direction. The pore morphology of the NAA-GPSs induces a modification in depth of the porosity, which in turn results in a variation of the refractive index in depth. The resulting system is a composition of multiple layers with varying constant refractive index between high and low values. The effective refractive index of each layer was calculated using the Looyenga-Landau-Lifshitz formula adapted to NAA-GPSs. The dimension in the Z direction of the 1D-effective graded-index system was determined by the physical thickness of one period ( $\Delta$ ) by the number of cycles (N). The optical source was an incident plane wave perpendicular to the surface of the structure (XY plane), which propagated perpendicular

to the Z axis from 350 to 1200 nm at an angle of incidence of 8°. The reflectance spectra were calculated by the TMM method, where the above multi-layered thin film model was implemented. Calculations were performed using a custom-designed program in MATLAB software.



**Figure 5.2**. Illustration of the transition of the NAA-GPSs pore morphology towards a multilayered system in which the constant effective refractive index of each layer varies between  $n_{low}$  and  $n_{high}$ .

#### 5.3. Results and Discussion

#### 5.3.1 Fabrication of NAA-GPSs

**Figure 5.3** shows a set of representative Gaussian pulse anodization profiles used to produce NAA-GPSs. Six types of NAA-GPSs were produced with fixed  $J_0 = 1.13$  mA cm<sup>-2</sup>,  $J_1 = 2.26$  mA cm<sup>-2</sup>, T = 250 s, N = 150 pulses, and systematically varied C = 5, 10, 20, 30, 40 and 60 s. **Table 5.1** summarizes the fabrication conditions of the assessed NAA-GPSs, labelled as NAA-GPS-1 (C = 5 s), NAA-GPS-2 (C = 10 s), NAA-GPS-3 (C = 20 s), NAA-GPS-4 (C = 30 s), NAA-GPS-5 (C = 40 s) and NAA-GPS-6 (C = 60 s) as a

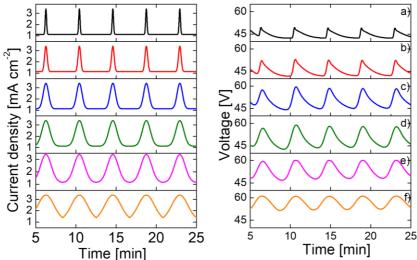
function of the value of C used in their fabrication. While the voltage anodization profile (output) shows an asymmetric Gaussian shape with the current density input for C= 5–30 s, it turns into a quasi-symmetric Gaussian bell for C > 30 s.

Analysis of the anodization profiles reveal the output voltage follows closely the input current density profile, with a delay of ~0.4 min. This short delay is attributable to the dynamic modification of the anodization current density, which disturbs the continuous flow of the electrolytic species across of the oxide barrier layer. Such alteration leads to a recovery time until the electrochemical equilibrium is reached again. <sup>37,51-52</sup> The voltage output profiles shown in **Figure 5.3** reveal voltage Gaussian pulses with asymmetric shape of Gaussian pulses, the asymmetry of which increases with decreasing width of the anodizing Gaussian current density pulse input. This phenomenon is due to the capacitor effect in the oxide barrier layer located at the nanopore bottom tips, which separates the electrolyte/oxide and the oxide/metal interfaces.

When the current density input is suddenly altered, the oxide barrier layer – an electrical insulator – accumulates charge carriers (electrons and electrolytic species). These charge carriers are slowly released during the voltage recovery time, when the current density input is reduced from high to low level. The reduction of current density input in wider Gaussian pulses is smoother than that of their counterparts with narrower width, which in turns minimizes the asymmetry of the Gaussian voltage pulse output.

**Table 5.1.** Summary of fabrication parameters used to produce Gaussian NAA-GPSs.

Sample	<b>J</b> <sub>0</sub> [mA cm <sup>-2</sup> ]	<b>J<sub>1</sub></b> [mA cm <sup>-2</sup> ]	<b>T</b> [s]	<b>N</b> [Pulses]	<b>C</b> [s]
NAA-GPS-1	1.13	2.26	250	150	5
NAA-GPS-2	1.13	2.26	250	150	10
NAA-GPS-3	1.13	2.26	250	150	20
NAA-GPS-4	1.13	2.26	250	150	30
NAA-GPS-5	1.13	2.26	250	150	40
NAA-GPS-6	1.13	2.26	250	150	60

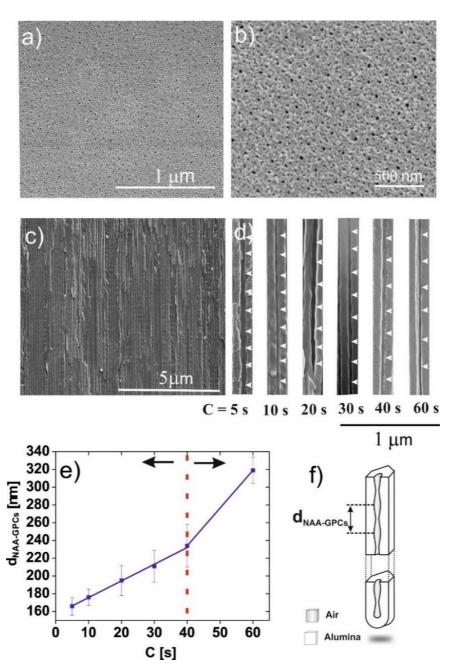


**Figure 5.3.** Analysis of Gaussian pulse anodizing current density (input) and voltage (output) profiles used to fabricate NAA-GPSs (NB: fixed anodization parameters  $-J_0 = 1.13 \text{ mA cm}^{-2}$ ,  $J_1 = 2.26 \text{ mA cm}^{-2}$ , T = 250 s and N = 150 pulses). (a) NAA-GPS-1 (C = 5 s). (b) NAA-GPS-2 (C = 10 s). (c) NAA-GPS-3 (C = 20 s). (d) NAA-GPS-4 (C = 30 s). (e) NAA-GPS-5 (C = 40 s). (f) NAA-GPS-6 (C = 60 s).

#### **5.3.2 Structural characterization of NAA-GPSs**

**Figure 5.4** shows representative FEG-SEM images of NAA-GPSs produced with  $J_0 = 1.13$  mA cm<sup>-2</sup>,  $J_1 = 2.26$  mA cm<sup>-2</sup>, T = 250 s, N = 150 pulses and C = 5, 10, 20, 30, 40 and 60 s. The general top view FEG-SEM image shows nanopores randomly distributed across the surface of the Gaussian NAA-PC (**Figure 5.4a**), the average diameter of which is ~17 nm (see a magnified top view with details of nanopores in **Figure 5.4b**). The general cross-sectional FEG-SEM image reveals nanopore diameter modulations along the nanopore length, which are induced by the input Gaussian current density pulses (**Figure 5.4c**). Nanopore diameter modulations are translated into effective medium modulations in depth, leading to the top—down generation of an 1D NAA-GPS structure. **Figure 5.4d** shows a cross-sectional view of the period length ( $d_{NAA-GPSs}$ ) in NAA-GPSs, as graphically defined in **Figure 5.4f**.

The period length corresponds to the length of the stacked layers of NAA generated during each Gaussian pulse. FEG-SEM analysis reveals that, for C = 5, 10, 20, 30, 40 and 60 s, the period length are  $166 \pm 10$ ,  $176 \pm 9$ ,  $195 \pm 17$ ,  $211 \pm 18$ ,  $234 \pm 24$ ,  $319 \pm 15$  respectively. **Figure 5.4.e** shows the dependence of  $d_{NAA-GPSs}$  with C, in which the former structural feature increased with the latter anodization parameter. This graph reveals two growth regimes, from C = 5 to 40 s and from 40 to 60 s. While the period length grows at a rate of 1.88 nm s<sup>-1</sup> within the first regime, it becomes more dependent on C > 40 s, which a growth rate of 4.25 nm s<sup>-1</sup>.



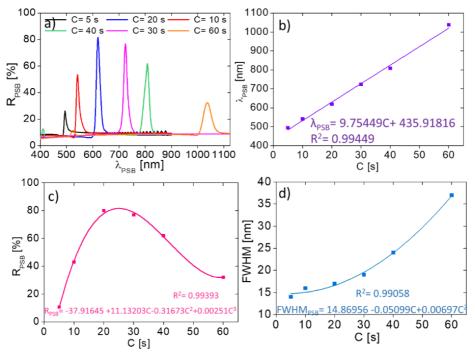
**Figure 5. 4.** Structural characterization of NAA-GPSs produced by Gaussian pulse anodization (NB: NAA-GPS produced with  $J_0$  = 1.13 mA cm<sup>-2</sup>,  $J_1$  = 2.26 mA cm<sup>-2</sup>, N = 150 pulses, T = 250 s and C = 5, 10,20, 30, 40 and 60 s). (a) General top view FEG-SEM image of a representative NAA-GPS (b) Magnified view of a representative NAA-GPS. (c) General cross-sectional FEG-SEM view of a representative NAA-GPS). (d) Cross-view of NAA-GPSs with C= 5, 10, 20, 30, 40 and 60 s. (e) relation between C and period length ( $d_{NAA-GPSs}$ ). (f) Illustration of period length of NAA-GPSs .

## **5.4 Optical Characterization of NAA-GPSs**

## 5.4.1 Effect of Gaussian Pulse Width on the Optical Features of the Characteristic PSB of NAA-GPSs

To study the effect of the Gaussian width (i.e. C parameter) on the optical properties of NAA-GPSs, a set of these PC structures was fabricated by Gaussian pulse anodization with fixed  $J_0 = 1.13$  mA cm<sup>-2</sup>,  $J_1 = 2.26$  mA cm<sup>-2</sup>  $^{2}$ , T = 250 s, N = 150 pulses, and varying C = 5, 10, 20, 30, 40 and 60 s. **Figure 5.5a** shows reflectance spectra of NAA-GPSs produced with C = 5, 10, 20, 30, 40 and 60 s, which feature narrow characteristic PSBs with an average full width at half maximum ( $FWHM_{PSB}$ ) of 21 ± 9 nm. It is apparent that the position of the PSB red-shifts with increasing C following a linear dependence, in which  $\lambda_{PSB}$  red-shifts at a rate of 9.8  $\pm$  0.3 nm s<sup>-1</sup> with C, with a linearity correlation coefficient of 0.994 (Figure 5.5b). Analysis of the anodization profiles shown in Figure 5.3 reveals that both the amplitude and offset of the anodizing voltage output increase with C. Previous studies have demonstrated that increasing voltage offset in NAA-PCs produced under current density control conditions results in a redshift in the characteristic PSB of the PCs<sup>30</sup> due to increment in the period length within the PC structure. Figure 5.5c shows the dependence between the maximum reflection intensity of the PSB of NAA-GPSs and C. It can observe that NAA-GPSs produced with C = 20 s achieve the maximum intensity ( $\sim$ 80%), whereas those NAA-GPSs produced with C=5s have the lowest intensity (~10%). A cubic polynomial fitting was used establish a correlation between the intensity of the PSB and C, which was found to describe precisely the dependence between optical feature and fabrication parameter, as denoted by the correlation coefficient of  $R^2$  =

0.995. **Figure 5.5d** depicts the relationship between  $FWHM_{PSB}$  of NAA-GPSs and C. This graph indicates that  $FWHM_{PSB}$  increases exponentially with increasing C, from 10 nm at C = 5 s (narrowest PSB) to 37 nm at C = 60 s (broadest PSB).



**Figure 5.5.** Effect of Gaussian width (*C*) on the features of the PSB of NAA-GPSs fabricated by Gaussian pulse anodization at fixed  $J_0 = 1.13$  mA cm<sup>-2</sup>,  $J_1 = 2.26$  mA cm<sup>-2</sup>, T = 250 s and N = 150 at  $\vartheta = 8^{\circ}$ . (a) Reflection spectra of NAA-GPSs as a function of C = 5, 10, 20, 30, 40 and 60 s. (b) Position of the reflection band of NAA-GPSs ( $\lambda_{PSB}$ ) (c) Intensity reflection ( $R_{PSB}$ ) of NAA-GPSs (d) Full width at half maximum ( $FWHM_{PSB}$ ) NAA-GPSs.

# 5.4.2 Effect of Angle of Incidence on the Optical Features of the Characteristic PSB of NAA-GPSs

The combinational effect of the incidence angle and C on the optical features of the characteristic PSB of NAA-GPSs was investigated. **Table 5.2** provides a detailed summary of the effect of each of these parameters on the optical features (i.e.,  $\lambda_{PSB}$ ,  $R_{PSB}$ ,  $FWHM_{PSB}$  and quality factor  $-Q_{PSB} = 1$ 

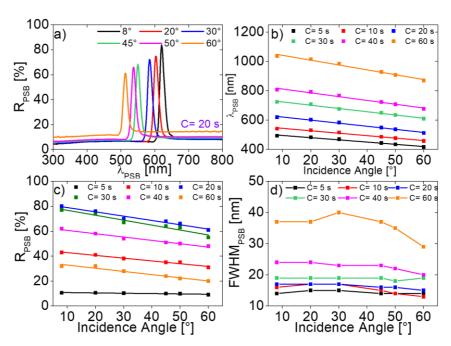
 $\lambda_{PSB}/$  FWHM<sub>PSB</sub>) of NAA-GPSs produced by Gaussian pulse anodization. **Figure 5.6a** shows the reflection spectra of a NAA-GPS-3 at different incidence angles ( $\vartheta$  = 8, 20, 30, 45, 50 and 60°). It is apparent that the position of the PSB of NAA-GPSs undergoes a blue-shift when the incidence angle increases. This result is in good agreement with the Bragg–Snell law, in which the wavelength of the diffracted light depends on the incidence angle, the periodicity and the effective refractive index<sup>36,53-57</sup> of the nanoporous PC, as expressed in Equation 2:

$$m\lambda_{PSB} = 2d_{NAA-GPCS} \sqrt{n_{eff}^2 - \sin^2\theta}$$
 (5.2)

where  $\lambda_{PSB}$  is wavelength of the PSB, m is the order of the PSB,  $d_{NAA-GPS}$  is the structure periodicity,  $\vartheta$  is the incidence angle,  $n_{eff}$  is the effective refractive index. **Figure 5.6b** shows that the position of the PSB of NAA-GPSs is shifted toward shorter wavelengths (i.e., blue-shift) with increasing incidence angle and increasing C, as revealed by linear fittings. Analysis of the fitting lines denotes that  $\lambda_{PSB}$  blue-shifts at rates of -1.51, -1.66, -2.10, -2.25, -2.59 and -3.30 nm/° for C = 5, 10, 20, 30, 40 and 60 s, respectively. Analysis of **Figure 5.6c** indicates that the reflection intensity of the PSB decreases as the incidence angle increases. Analysis of the fitting lines denotes that  $R_{PSB}$  decreases at rates of -0.02, -0.03, -0.39, -0.34, -0.27 and -0.25 %/° for C = 5, 10, 20, 30, 40 and 60 s, respectively. **Figure 5.6d** shows the  $FWHM_{PSB}$  dependence with the angle of incidence. It is apparent that the  $FWHM_{PSB}$  remains almost constant when the incidence angle increases.

**Table 5.2**. Summary of the effect of C parameter and the incidence angle on the reflectance spectrum of Gaussian NAA-PCs.

Sample	Parameter	8°	20°	30°	45°	50°	60°
G1 C= 5s	λ <sub>PSB</sub> [nm]	494	483	470	444	435	417
	R <sub>PSB [%]</sub>	10.6	10.6	10.3	10	9.9	9.09
	FWHM <sub>PSB</sub> [nm]	14	15	15	14	14	13
	$Q_{PSB}$	31	28	27	29	30	34
	λ <sub>PSB</sub>	542	531	516	487	477	458
G2	R <sub>PSB</sub> [%]	43	41	38	35	35	31
C= 10s	FWHM <sub>PSB</sub> [nm]	16	17	17	15	14	13
	$Q_{PSB}$	39	35	35	34	33	34
	$\lambda_{PSB}$	620	603	584	550	537	512
G3 C= 20s	R <sub>PSB [%]</sub>	80	76	70	68	66	61
	FWHM <sub>PSB</sub> [nm]	17	17	17	16	16	15
	Q <sub>PSB</sub>	39	35	35	34	33	34
	λ <sub>PSB</sub>	724	709	676	655	635	610
G4	R <sub>PSB</sub> [%]	77	74	67	64	63	55
C= 30s	FWHM <sub>PSB</sub> [nm]	19	19	19	19	18	19
	Q <sub>PSB</sub>	40	37	35	35	35	32
G5 C= 40s	λ <sub>PSB</sub>	808	792	768	723	708	677
	R <sub>PSB [%]</sub>	62	58	54	51	50	48
	FWHM <sub>PSB</sub> [nm]	24	24	23	23	22	20
	$Q_{PSB}$	34	33	33	31	32	33
G6 C= 60s	λ <sub>PSB</sub>	1037	1016	985	929	908	870
	R <sub>PSB [%]</sub>	32	32	28	24	22	20
	FWHM <sub>PSB</sub> [nm]	37	37	40	37	35	29
	$Q_{PSB}$	28	27	24	25	26	30



**Figure 5.6** Combinational effect of incidence angle and Gaussian width on the PSB's features of NAA-GPSs (NB: NAA-GPSs produced at fixed  $J_0$  = 1.13 mA cm<sup>-2</sup>,  $J_1$  = 2.26 mA cm<sup>-2</sup>, T = 250 s and N = 150, and varying C = 5, 10, 20, 30, 40 and 60 s and  $\vartheta$  = 8, 20, 30, 45, 50 and 60°). (a) Representative reflection spectra of NAA-GPS-3 (C = 20 s) at varying  $\vartheta$ . (b) Position of PSB ( $\lambda_{PSB}$ ) as a function of C and  $\vartheta$ . (c) Reflection intensity of PSB ( $R_{PSB}$ ) as a function of C and  $\vartheta$ . (d) Full width at half maximum of PSB ( $FWHM_{PSB}$ ) as a function of C and  $\vartheta$ .

# 5.4.3 Effect of Pore Widening on the Optical Features of the Characteristic PSB of NAA-GPSs

To assess the effect of the internal porosity on the optical properties of NAA-GPSs, the nanopores of a set of these PC structures, fabricated with  $J_0 = 1.13 \text{ mA cm}^{-2} J_1 = 2.26 \text{ mA cm}^{-2}$ , T = 250 s, C = 20 s and N = 150 pulses, were widened by wet chemical etching at different pore widening times ( $t_{pw} = 0$ , 5, 10, 15 and 20 min). ESEM image analysis established a direct correlation between  $t_{pw}$  and the nanopores diameter, which was found to be ~20, 30, 40, 50, 60 nm at  $t_{pw} = 0$ , 5, 10, 15 and 20 min, respectively (**Figure 5.7**).

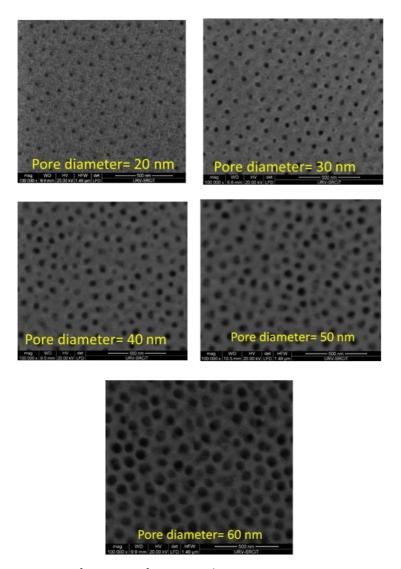
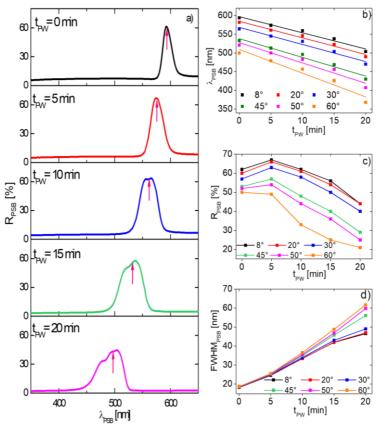


Figure 5.7. Top view of NAA-GPS after Pore widening treatment

**Figures 5.8a–d** show the dependence of  $\lambda_{PSB}$ ,  $R_{PSB}$  and  $FWHM_{PSB}$  of the characteristic PSB of NAA-GPSs with  $t_{pw}$ . **Figure 5.8a** shows the reflection spectra of a representative NAA-GPS (C=20~s) with  $t_{pw}$ , from 0 to 20 min. It is apparent that the position of the characteristic PSB in the reflection spectrum of NAA-GPSs is blue-shifted when their nanoporous structure is widened. The reflection band is shifted toward shorter wavelengths due to the reduction of the fraction of alumina ( $n_{Alumina} \sim 1.7~\text{RIU}$ ) with respect

to air ( $n_{air}$  = 1.0 RIU) in the effective refractive index of the PC structure. **Figure 5.8b** shows the dependence of  $\lambda_{PSB}$  with  $t_{pw}$ , in which the former optical feature is blue-shifted with the latter fabrication parameter at a rate of  $-5.7 \pm 0.4$  nm min<sup>-1</sup>. **Figure 5.8c** shows the dependence of  $R_{PSB}$  with  $t_{pw}$ . This behavior is observed for all angles of incidence measured. **Figure 5.8d** shows the dependence of  $FWHM_{PSB}$  with  $t_{pw}$ , in which this optical feature increases at a rate of 1.48 nm min<sup>-1</sup> as the nanoporous structure is widened.



**Figure 5.8.** Effect of pore widening time ( $t_{PW} = 0$ , 5, 10, 15 and 20 min) on the optical features of the PSB of NAA-GPSs (NB: NAA-GPSs produced at fixed  $J_0 = 1.13$  mA cm<sup>-2</sup>,  $J_1 = 2.26$  mA cm<sup>-2</sup>, T = 250 s and N = 150 and  $\vartheta = 8$ , 20, 30, 45, 50 and 60°). (a) Representative reflection spectrum of a NAA-GPS produced with C = 20 s at  $\vartheta = 8$ ° as a function of  $t_{PW}$  from 0 to 20 min. (b) Linear fitting lines showing the dependence between  $\lambda_{PSB}$  and  $t_{PW}$ . (c) Lines showing the dependence between  $FWHM_{PSB}$  and  $t_{PW}$ .

#### 5.4.4 Assessment of Effective Medium of NAA-GPSs

In order to evaluate the optical sensitivy of NAA-GPSs, spectral shifts in the characteristic PSB of these PCs upon infiltration of their nanoporous network with double-distilled water-based D-glucose solutions of varying concentration (i.e. 0.0125, 0.0250, 0.050, 0.125, 0.250, 0.50, 0.75 and 1.0 M) were measured in real-time using a flow system. The correlation between D-glucose concentration and refractive index is show in **Figure 5.9.** 

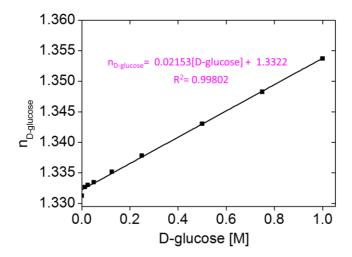


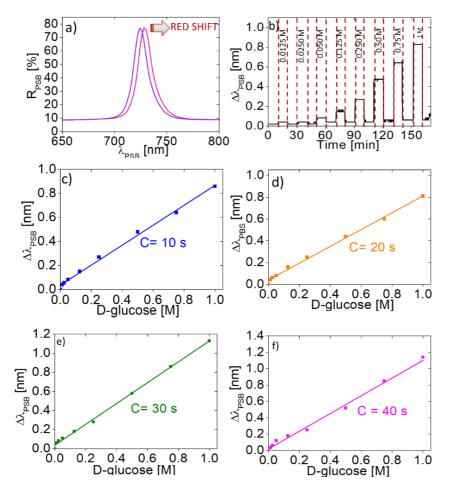
Figure 5.9. Correlation between D-glucose concentration and refractive index

Dynamic variations of the refractive index of the medium inside the nanopores shift in the position of the PSB of NAA-GPSs (i.e. increment in refractive index – red shift; decrement in refractive index – blue shift) (Figure 5.10a). Figure 5.10b illustrates a representative example of real-time monitoring of PSB shifts in a NAA-GPS-2 upon infiltration of its nanoporous structure with analytical solutions of D-glucose. First, a stable baseline was obtained by flowing water for 10 min.

Then, analytical solutions of D-glucose with varying concentration (0.0125, 0.0250, 0.050, 0.125, 0.250, 0.50, 0.75 and 1.0 M) were flowed through the system at 500  $\mu$ L min<sup>-1</sup>. Washing steps with fresh doble-distilled water were introduced between each analytical solution to remove remaining glucose molecules from the nanopores. The infiltration of the nanoporous structure of NAA-GPSs with aqueous solutions of D-glucose of increasing refractive index red-shifts the position of the characteristic PSB to longer wavelengths. The position of the PSB returns to its original baseline when water is flowed through the system, indicating that changes in the effective medium of these PSs are exclusively attributable to alterations in the refractive index of the medium filling the nanopores, without permanent chemical interaction between the inner surface of NAA-GPSs and glucose molecules in the analytical solution.

**Figures 5.10c–f** summarize linear correlations between the concentration of D-glucose and the red-shift of the PSB of NAA-GPS-2–NAA-GPS-5, and **Table 5.3** compiles the values of the most representative sensing parameters. The sensitivitie (*S*) of NAA-GPS-2–5, expressed in terms of slope of these linear fittings, were  $0.83 \pm 0.02$ ,  $0.77 \pm 0.02$ ,  $1.04 \pm 0.02$  and  $1.08 \pm 0.05$  nm M<sup>-1</sup>, respectively. These results indicate that the most sensitive NAA-GPS structure is that produced with *C* = 40 s. The low limit of detection (LOD–  $3\sigma$  = 3 times the standard deviation of the lowest D-Glucose concentration divided by S) was found for the sample *C* = 10 s. These NAA-GPSs show excellent linearity (R<sup>2</sup> – correlation coefficient) with an average of 0.994.

**Table 5.4** provides a summary compiling the sensing performance of the most relevant examples combining NAA-PCs in real -time for sensing application using D-glucose.



**Figure 5.10.** Effective medium assessment of NAA-GPSs. (a) Reflection spectrum of NAA-GPSs in water (purple) and D-Glucose (pink) showing the sensing principle (red-shift) used in Real-time experiments (b) Representative real-time shits in  $\lambda_{PSB}$  of NAA-GPSs upon selective infiltration of their nanoporous structure with analytical solutions of D-glucose with varying concentration, from 0.0125 to 1.0 M (NB: NAA-GPS produced at fixed  $J_0$  = 1.13 mA cm<sup>-2</sup>,  $J_1$  = 2.26 mA cm<sup>-2</sup>, T = 250 s and N = 150, C = 10 and  $\vartheta$  = 0°. (c–f). Linear correlations summarizing the dependence between  $\lambda_{PSB}$  in NAA-GPSs (C = 10. 20, 30 and 40 s) and D-glucose concentration.

**Table 5.3.** Sensitivity and low limit of detection of NAA-GPSs produced by Gaussian pulse anodization upon infiltration of their effective medium with analytical solutions of D-glucose.

Sample	S [nm M <sup>-1</sup> ]	LOD [mM]	R <sup>2</sup>
NAA-GPS-2 (C = 10 s)	0.83 ± 0.02	7.49 ± 0.26	0.995
NAA-GPS-3 (C = 20 s)	0.77 ± 0.02	16.3 ± 0.18	0.994
NAA-GPS-4 (C = 30 s)	1.04 ± 0.02	28.8 ± 0.20	0.997
NAA-GPS-5 (C = 40 s)	1.08 ± 0.05	29.6 ± 0.32	0.985

**Table 5.4.** Comparison of the sensing performance for different NAA-PCs

NAA Structure	Analyte	LOD [mivi]	3	Reference
NAA-GPS	D-Glucose	7.49-29.6	0.77-1.08 [nm M <sup>-1</sup> ]	This work
Rugate Filters	D-Glucose	10-15	1.95-4.93 [nm M <sup>-1</sup> ]	12
DBR	D-Glucose	0.0042	0.0115 % [μM <sup>-1</sup> ]	58
Fabry- Pérot	D-Glucose	100	0.007 % [mM <sup>-1</sup> ]	59

To validate the experimental results, we adapted the Looyenga–Landau–Lifshitz (3L) EMA model to describe the distribution of effective refractive index in NAA-GPSs. This model can be easily implemented to describe the effective medium of composite photonic crystal systems. In particular, the Looyenga–Landau–Lifshitz model adapted to NAA-GPSs can be expressed by Equation 5.3<sup>49-57</sup>.

$$n_{eff-NAA-GPCS}^{\frac{2}{3}} = f_{Al_2O_3} * n_{Al_2O_2}^{\frac{2}{3}} + f_{med} * n_{medium}^{\frac{2}{3}}$$
 (5.3)

where  $n^{2/3}_{eff\text{-}NAA\text{-}GPSs}$  is the effective refractive index of NAA-GPSs,  $n^{2/3}_{Al2O3}$ , is the refractive index of alumina,  $f_{medium}$  volume fraction of filling medium,  $n^{2/3}_{medium}$  is the refractive index of filling medium, and  $f_{Al2O3}$  is the volume fraction of alumina.

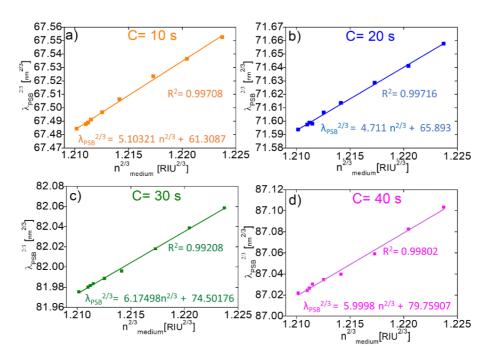
Furthermore, the reflection of light in each layer of NAA within the structure of NAA-GPSs follows the Fabry-Perót relationship shown in Equation 5.4:

$$\lambda_{PSB} = 2n_{eff-NAA-GPCS} * d_{NAA-GPCS} * \cos \theta$$
 (5.4)

where  $\lambda_{PSB}$  is the position of the PSB,  $n_{eff\text{-}NAA\text{-}GPSs}$  is the effective refractive index of NAA-GPSs,  $d_{NAA\text{-}GPSs}$  in the period length and  $\vartheta$  is the incidence angle of light. Equation 5.4 can be reorganized as Equation 5.5 taking into account  $f_{Al2O3} + f_{med} = 1$  and  $\theta = 0^\circ$ :

$$\lambda_{PSB} = (2d_{NAA-GPCS})^{\frac{2}{3}} * (1 - f_{med}) * n_{Al_2O_3}^{\frac{2}{3}} + 2d_{NAA-GPCS}^{\frac{2}{3}} * f_{med} * n_{med}^{\frac{2}{3}}$$
 (5.5)

**Figure 5.11** shows the obtained values and linear fittings after substituting the experimental data in the 3L model adapted for NAA-GPSs. A linear fitting between  $\lambda_{PSB}^{2/3}$  and  $n^{2/3}_{medium}$  made it possible to estimate  $d_{NAA-GPSs}$  and  $f_{medium}$ , which for instance were found to be 170  $\pm$  5 nm and 0.11  $\pm$  0.02 for NAA-GPS-2, respectively. This result is in good agreement with simulations using the transfer matrix method, which gave an estimation for  $d_{NAA-GPSs}$  of 160 nm (i.e., ~6% deviation between experimental and simulated results). This result demonstrates that the effective medium of NAA-GPSs produced by Gaussian pulse anodization can be precisely described by the 3L EMA model. The comparison of experimental data and simulations is summarized in **Table 5.5** and **Table 5.6**, respectively. **Figure 5.12** shows a direct comparison between simulated and experimental reflection spectra of NAA-GPSs assessed in this study. It is apparent that simulated (blue lines) and experimental (red lines) spectra of NAA-GPS-2, NAA-GPS-4 and NAA-GPS-5 are in excellent agreement.



**Figure 5.11.** Assessment of effective medium of NAA-GPSs using the Looyenga-Landau-Lifshtz model (3L) (NB: NAA-GPS produced at fixed  $J_0 = 1.13$  mA cm<sup>-2</sup>,  $J_1 = 2.26$  mA cm<sup>-2</sup>, T = 250 s, N = 150 pulses and varying C). (a) C = 10 s. (b) C = 20 s. (c) C = 30 s. (d) C = 40 s.

**Table 5.5** Comparison of the experimental results.

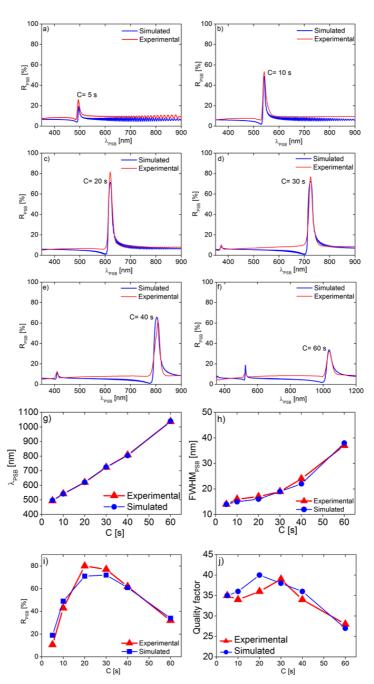
	Looyenga-Landau-Lifshitz		Optical				Structural			
	model			Characterization				characterization		
C [s]	d <sub>NAA GAUSS</sub> [nm]	f medium [%]	L <sub>NAA-GPCs</sub> [nm]	λ <sub>PSB</sub> [nm]	FWHM <sub>PSB</sub> [nm]	Q	R <sub>PSB</sub> [%]	Pore diameter [nm]	Porosity [%]	L <sub>Total</sub> [nm]
5	-	-	-	494	14	35	10.6	17	10.3	
10	170	10.5	25500	542	16	34	43	17	11.3	22800
20	185	10.5	27750	620	17	36	80	17	9.5	24100
30	227	10.5	34050	724	19	39	77	17	9.1	30500
40	248	9.5	37200	808	24	34	62	17	9.3	34200
60	-	ı	-	1037	37	28	32	17	10	

**Table 5.6** Comparison of the simulation results.

C [s]	d <sub>NAA</sub> GAUSS [nm]	λ <sub>PSB</sub> [nm]	FWHM <sub>PSB</sub> [nm]	Q	R <sub>PSB</sub> [%]	f medium [%]	L <sub>total</sub> [nm]
5	145	497	14	35	19	10	21750
10	160	542	15	36	49	10	24000
20	185	621	16	40	71	10	27500
30	217	725	19	38	72	10	32550
40	240	804	22	36	61	10	36000
60	305	1040	38	27	34	10	45750

This result further demonstrates that the transfer matrix model developed in this study can be precisely predict the reflection bands of NAA-GPSs. **Figures 5.12g–j** compiles a comparative summary of the experimental (triangles) and simulation (circles) results for  $\lambda_{PSB}$ ,  $FWHM_{PSB}$ ,  $R_{PSB}$  and  $Q_{PSB}$  as a function of C. **Figure 5.12g** shows the experimental and simulated values of  $\lambda_{PSB}$  for NAA-GPS-1 to NAA-GPS-6. These data demonstrate that simulations can predict the spectral position of the PSB of NAA-GPSs with excellent accuracy, with almost negligible deviations of 0.60% (C = 5 s), 0.00% (C = 10 s), 0.16% (C = 20 s), 0.13% (C = 30 s), 0.49% (C = 40 s), and 0.29% (C = 60 s).

**Figure 5.12h** shows a comparative analysis between experimental and simulated values for  $FWHM_{PSB}$ . These results show a close correlation between experimental and simulated values, with a small average deviation of ~3.8%. It is also apparent that our model can precisely describe the intensity of the PSB for C = 30-60 s, with a deviation ranging between 1.6–6.9% (**Figure 5.12i**).



**Figure 5.12.** Effective medium model validation through comprehensive comparison between experimental values and simulation estimations for NAA-GPSs (NB: red lines and dots – experimental values; blue lines and dots – simulated estimations). (a–f) Experimental and simulated reflection spectra of NAA-GPSs as a function of C=5, 10, 20, 30, 40 and 60 s. (g) Comparison between experimental and simulated values for  $\lambda_{PSB}$  at C=5-60 s. (i) Comparison between experimental and simulated values for  $FWHM_{PSB}$  at C=5-60 s. (j) Comparison between experimental and simulated values for  $R_{PSB}$  at C=5-60 s. (j) Comparison between experimental and simulated values for  $R_{PSB}$  at C=5-60 s.

However, discrepancy between simulations and experimental values is observed with a ~14.1% deviation at C=20 s. Comparison between experimental and simulated estimations of  $Q_{PSB}$  for NAA-GPSs is shown in **Figure 5.12j**. Small discrepancy between experimental values and simulated estimations are observed with an average deviation ~3.4%. However, a disagreement of 10% is found for NAA-GPSs produced with C=20 s. To summarize, analysis of the optical features of NAA-GPSs estimated from experimental data and simulations further demonstrate that our effective medium model can precisely describe the optical properties of these PC structures, providing new opportunities to design high-quality NAA-GPSs with tunable PSBs across the visible—NIR spectrum.

### 5.5. Conclusion

In this chapter, we fabricated photonic crystals based in nanoporous anodic alumina using a novel pulse-like anodization approach consisting of current density Gaussian pulses. The effect of the Gaussian pulse width on the optical features of the characteristic photonic stopband of these nanoporous PCs —position of central wavelength, full width at half maximum, reflection intensity and quality factor— was systematically assessed at varying angle of incidence. The position of the PSB of these PCs can be precisely tuned varying by the width of the Gaussian pulse, from  $\lambda_{PSB} = 494$  nm to 1037 nm from C = 5 to 60 s, respectively. The reflection presented a highest intensity when C = 20 s (80%) and lowest when C = 5 s (20%) and  $FWHM_{PSB}$  increase exponentially when C increases. Furthermore, we evaluated the effect of the angle of incidence angle in the reflection bands and we observe a blue-shift when the incidence angle

increases according with the Bragg-Snell law. The reflection intensity was also affected, as the incidence angle increases the intensity decreases. The FWHM<sub>PSB</sub> was not affected for the incidence angle. In addition, we report the effect of the porosity of the Gaussian-NAA-GPSs applying a pore widening chemical etching from 0 to 20 minutes increasing the nanopore diameter from 20 to 60 nm. The position of the reflection band blueshifted from 594 to 495 nm also was observed an increment in the intensity and the width of the reflection bands. The potential applicability of these PC structures as optical platform for sensing applications was evaluated by monitoring in real-time spectral shifts in their characteristic PSB upon selective infiltration of their medium with analytical solutions of D-glucose. These observations indicate that NAA-GPSs can achieve high optical sensitivity (1.08  $\pm$  0.05 nm M<sup>-1</sup>), low limit of detection (7.5  $\pm$  0.26 mM) and excellent linearity ( $R^2 = 0.994$ ). We also demonstrated that the effective medium of NAA-GPSs can be mechanistically explained by the Looyenga-Landau-Lifshitz EMA model, as confirmed by correlations between experimental data and model predictions of structural parameters ( $d_{NAA-GPSs}$  and  $f_{medium}$ ). The experimental observations were further validated and mechanistically described by developing a theoretical effective medium model, using the transfer matrix approach, and performing a comprehensive comparison between experimental values and simulated estimations. The model can be used to precisely predict the experimental data and optical features of NAA-GPSs, opening exciting opportunities to engineer innovative PCs architectures for specific light-based applications.

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Chapter 6. Photonic Crystals

Microcavities: Fabrication,

Chemical surface sensitivity

and light confining

UNIVERSITAT ROVIRA I VIRGILI ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla In this Chapter Nanoporous anodic alumina optical microcavities (NAA– $\mu$ QVs) with spectrally tunable resonance band and surface chemistry are used as model light-confining photonic crystal (PC) platforms to elucidate the combined effect of spectral light confinement features and surface chemistry on optical sensitivity nm<sup>-1</sup> in water- and organic-based analytical solutions, respectively. These advances provide new insights into critical factors determining optical sensitivity in light-confining nanoporous PC structures, with implications across optical sensing applications, and other photonic technologies.

# **6.1 Introduction**

Photonic crystals (PCs) are a class of structured materials that enable precise molding of electromagnetic waves flow for a plethora of applications. <sup>1,2</sup> Light propagation across PCs is governed by interference between multiply Bragg scattered waves, the energy dispersion of which is formally described by a photonic band diagram featuring allowed and forbidden bands. <sup>3</sup> As such, PCs enable precise control over a variety of light–matter interactions by engineering their architecture, composition, and structural features. <sup>4,5</sup> Of all forms of light–matter interactions, confinement of light is an indispensable process for a wide range of applications such as astrophysics <sup>6</sup>, quantum computing <sup>7,8</sup>, lasing <sup>9</sup>, telecommunications <sup>10</sup>, and sensing <sup>11</sup>. Optical microcavities are a type of PCs that confine light into small volumes by resonant recirculation of electromagnetic waves. <sup>12,13</sup>

Strong light confinement within these PC structures is characterized by a narrow, well-resolved spectral resonance band (RB), the width of which would ideally correspond to a single wavelength. However, in practice, the

resonance band of optical microcavities spans a relatively narrow range of wavelengths due to energy loss per optical cycle associated with structural defects and optical absorption. Similarly, minute perturbations of the environment within optical microcavities introduce changes in the properties of confined light, either in linewidth, frequency shift, or resonance splitting.<sup>14</sup> These alterations of confined waves are characteristically proportional to the induced perturbation magnitude, making optical microcavities prime candidates for many daily life sensing applications such as magnetometers for mineral exploration<sup>15</sup>, optomechanical transducers in mobile phones<sup>16</sup>, and single-particle/molecule detectors for environmental and medical diagnosis<sup>17,18</sup>. Porous optical microcavities are particularly suitable transducers for sensing since these PCs provide light-confining capabilities, high surface-to-volume ratio to increase functional binding sites and frequency of molecule-to-surface interactions, and nanochannels that facilitate transport of analyte molecules to minimize detection time. 19 1D nanoporous optical microcavities can be prepared with precisely engineered optical properties across the broad spectrum, from UV to IR, by anodization electrochemical oxidation. This top-down nanofabrication technique is also simple, cost-competitive, scalable, and controllable.<sup>20-22</sup> Porous silicon-based optical microcavities produced by anodization of silicon are the most mature and controllable technology to date. Recent advances in pulse-like anodization of aluminum have realized several architectures of nanoporous anodic alumina-based optical microcavities (NAA-μQVs).<sup>23-30</sup> However, only a few studies have explored the potential of these emerging optical transducers as sensing platforms. Yan et al. 28 and Lee et al.<sup>25</sup> demonstrated that NAA–μQVs are sensitive PC structures to changes

in refractive index, while Wang *et al.* proved that NAA– $\mu$ QVs' RB undergoes dynamic spectral shifts upon exposure to humidity from water vapor. Despite these advances, there remain fundamental questions concerning the design and engineering of NAA– $\mu$ QVs to maximizing sensitivity of light confined within their structure for practical sensing applications. Previous studies on nanoporous PCs<sup>31,32</sup> point that sensitivity of NAA– $\mu$ QVs is critically determined by i) size of analyte molecules, ii) degree to which analyte molecules increase the refractive index of the medium filling the nanopores, iii) molecule-to-surface interaction strength, and iv) spectral position and quality of light confinement.

Herein, the combined effect of spectral light confinement features and surface chemistry on optical sensitivity of NAA-µQVs has been analyzed for the first time. The architecture of these 1D NAA-PC structures is engineered by stepwise pulse anodization (STPA) under current density control conditions (Figure 6.1a). Model NAA-µQVs feature two highly reflective distributed Bragg mirrors with a physical cavity layer in between (Figure 6.1b). The optical spectrum of NAA-μQVs show well-resolved, spectrally tunable RBs, the central wavelength of which is engineered from ~400 to 800 nm by STPA (Figure 6.1c). The surface chemistry of NAAµQVs is selectively modified to alter their wettability. The characteristic RB of hydrophilic and hydrophobic NAA-µQVs undergoes quantifiable spectral shifts upon infiltration of their nanoporous structure with organic- and aqueous-based analytical solutions of equally varying refractive index. Analysis of refractive index-induced spectral shifts of NAA-μQVs' RB allows us to generate fundamental knowledge about how spectral resonance features and surface chemistry determine optical sensitivity in these model optical microcavities.

light confining

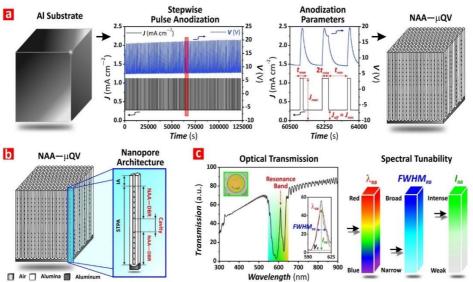


Figure 6.1. Fabrication and optical engineering of nanoporous anodic alumina optical microcavities (NAA- $\mu$ QVs) by stepwise pulse anodization (STPA). (a) Schematic of the fabrication process of NAA- $\mu$ QVs by STPA under current density control conditions with: aluminum substrate (left), representative STPA profile with a definition of anodization parameters (center), and idealized structure of NAA-µQVs (right) (NB: anodization profile used to produce a NAA- $\mu$ QV<sub>600</sub>, with a magnified view of red rectangle defining graphically the main anodization parameters including maximum current density  $-J_{max}$  = 1.120 mA cm<sup>-2</sup>, minimum or offset current density –  $J_{min} = J_{off} = 0.280$  mA cm<sup>-2</sup>, time at  $J_{max} - t_{max} = 160$  s, and time at  $J_{min} - t_{min} = 962$  s). (b) Schematic representing the idealized nanopore architecture of NAA- $\mu$ QVs formed by two NAA distributed Bragg reflectors (NAA-DBRs) with a physical cavity in between (NB: IA = initial anodization). (c) Representative transmission spectrum of a NAA-µQV600 showing details of the characteristic resonance band (RB) and a graphical description of the main optical features (inset) including central wavelength position  $-I_{RB}$ , full width at half maximum - $FWHM_{RB}$ , and intensity  $-I_{RB}$ , which can be precisely tuned across the UV-visible spectrum by the input anodization period in the STPA profile.

# **6.2 Experimental Details**

# 6.2.1. Fabrication of NAA– $\mu$ QVs by STPA.

 $1.5 \times 1.5$  cm square Al chips were cleaned in ethanol and water under sonication for 15 min each, dried, and stored until further use. Prior to anodization, Al chips were electropolished in a 4:1 (v:v) EtOH:HClO<sub>4</sub> electrolyte at 5 °C and 20 V for 3 min. After electropolishing, Al chips were anodized under current density control conditions in 1 M aqueous H<sub>2</sub>SO<sub>4</sub>

acid electrolyte at -2 °C. The acid electrolyte composition was modified with 25 v% of EtOH to prevent it from freezing at sub-zero temperature.33,34 Electrolyte temperature inside custom-built electrochemical reactors was kept constant throughout anodization, using a system of cold plates connected to liquid refrigerated circulators (AC150-A25, Thermo Fisher Scientific, Australia). The anodizing electrolyte was stirred at a rate of ~300 rpm to homogenize the temperature and composition of the reactant solution during anodization. The anodization process started with a constant current density (J) step at 1.120 mA cm<sup>-2</sup> for 10 min to achieve a constant nanopore growth rate before switching anodization to STPA. After that, this top-down fabrication process started with the generation of a NAA-DBR featuring a total of 55 NAA stacks with a stepwise modulated porosity. This structure was fabricated by switching the input current density between  $J_{max} = 1.120$ mA cm<sup>-2</sup> and  $J_{min} = J_{off} = 0.280$  mA cm<sup>-2</sup> in a stepwise fashion, for a duration of  $t_{max}$  and  $t_{min}$ , respectively, and for a total of 55 STPA pulses. Then, a physical cavity layer featuring straight nanopores was created by applying a constant current density step at  $J_{max} = J_Q = 1.120$  mA cm<sup>-2</sup>, for a given time of  $t_Q = 2 \cdot t_{max}$ . The process was then switched back to STPA mode to create another NAA-DBR structure with as many NAA stacks as those of the top NAA-DBR, under the same fabrication conditions. Input current density-time STPA profiles were generated by a custom-designed Labview-based application. The anodization period  $(T_P)$  for each STPA pulse was defined as the total time duration at  $J_{max}$  and  $J_{min}$ , where  $T_P =$  $t_{max} + t_{min}$  and  $t_{max} = 6 \cdot t_{min}$ . **Table 6.1** summarizes the conditions used to fabricate the five types of NAA-μQVs assessed in this study.

**Table 6.1.** Fabrication conditions used to produce NAA– $\mu$ QVs by STPA including anodization period ( $T_P$ ), maximum current density ( $J_{max}$ ), minimum current density ( $J_{min}$ ), time at  $J_{max}$  ( $t_{max}$ ), time at  $J_{min}$  ( $t_{min}$ ), cavity current density ( $J_Q = J_{max}$ ), and time at  $J_Q$  ( $t_Q$ ).

NAA-μQV	T <sub>P</sub> (s)	t <sub>max</sub> (s)	t <sub>min</sub> (s)	t <sub>Q</sub> (s)
		J <sub>max</sub> (mA cm <sup>-2</sup> )	J <sub>min</sub> (mA cm <sup>-2</sup> )	J <sub>Q</sub> (mA cm <sup>-2</sup> )
NAA-	748	107	641	214
μQV <sub>400</sub>		1.120	0.280	1.120
NAA-	935	134	801	268
μ <b>QV</b> <sub>500</sub>		1.120	0.280	1.120
NAA-	1122	160	962	320
μQV <sub>600</sub>		1.120	0.280	1.120
NAA-	1309	187	1122	374
μ <b>QV</b> <sub>700</sub>		1.120	0.280	1.120
NAA-	1496	214	1282	428
μQV <sub>800</sub>		1.120	0.280	1.120

# **6.2.2.** Surface Functionalization of NAA-μQVs.

The inner surface of a set of freshly prepared NAA-µQVs was chemically functionalized with dichlorodimethysilane via chemical vapor deposition.<sup>35</sup> In brief, NAA–μQVs were hydroxylated in 30 wt % H<sub>2</sub>O<sub>2</sub> at 100 °C for 10 min and dried under air stream. Hydroxylated NAA-μQVs were subsequently functionalized with dichlorodimethysilane by chemical vapor deposition under vacuum at 110 °C for 3 h. After this, NAA-μQVs were washed with ultrapure water and ethanol to remove unbounded dichlorodimethysilane molecules. Contact angle of as-produced and dichlorodimethysilane-functionalized NAA-µQVs was measured by an optical tensiometer (Attension Theta Flex, Biolin Scientific, Sweden), using the sensile drop technique. Briefly, a water droplet (~15 mL) was formed on the end of a syringe and approached to NAA-µQVs' surface until contact. Upon contact, the needle was withdrawn, and image analysis was performed to establish the contact angle on the surface of NAA-µQVs.

## 6.2.3. Optical Characterization of NAA-μQVs.

Before optical characterization, Al substrate remaining after fabrication was selectively removed from the backside of NAA-µQVs by wet chemical etching in a mix HCl-CuCl<sub>2</sub> solution (2.4 M HCl and 0.2 M CuCl<sub>2</sub>) to create a transparent window, using a 5 mm-diameter circular etching mask. Transmission spectra of NAA-µQVs were acquired at normal incidence, from 200 to 900 nm, using a UV-visible spectrophotometer (Cary 300, Agilent, USA). Optical features of the characteristic resonance band (RB) in the transmission spectra of NAA- $\mu$ QVs (i.e., central wavelength –  $\lambda_{RB}$ , full width at half maximum –  $FWHM_{RB}$ , intensity –  $I_{RB}$ , and quality factor –  $Q_{RB} = \lambda_{RB}/FWHM_{RB}$ ) were estimated from Gaussian fittings performed in OriginPro 8.5, using the lower lobe of the RB as a baseline  $(y_0)$ —graphical description in **Figure 6.1c**. The anodic oxide growth rate ( $G_R$ ) and effective refractive index ( $n_{eff}$ ) of NAA stacks forming the structure of NAA- $\mu$ QVs were quantified by a set of reference NAA films produced under constant current density control conditions at J<sub>min</sub> and J<sub>max</sub>, using 1 M H<sub>2</sub>SO<sub>4</sub> acid electrolyte at -2 °C.

The growth rate of NAA at  $J_{min}$  and  $J_{max}$  (i.e.  $G_{R-min}$  and  $G_{R-max}$ ) was determined via FEG-SEM image analysis from reference NAA films produced in 1 M H<sub>2</sub>SO<sub>4</sub> acid electrolyte at -2 °C for 5, 10, 15, and 20 h. NAA films used to characterize the effective refractive index of NAA at  $J_{min}$  and  $J_{max}$  (i.e.  $n_{eff-min}$  and  $n_{eff-max}$ ) were fabricated for a fixed total charge density of 5 C cm<sup>-2</sup>—integrated current density per unit area and time. Specular reflection spectra from these NAA films were acquired at varying

angles of incidence ( $q_{inc}$  = 15°, 25°, 35° and 45°) in a system comprising a variable angle reflection stage (RSS–VA, Ocean Optics, USA) coupled to a miniature visible optical fiber spectrometer (FLAME–T–VIS–NIR–ES, Ocean Optics, USA) and a tungsten light source (LS–1LL, Ocean Optics, USA) via optical fibers (QP200–2–UV–VIS, Ocean Optics, USA). Reflection spectra, from 400 to 900 nm, were acquired with an integration time of 10 ms and 20 average measurements, and processed by applying fast Fourier transform (FFT) in IgorPro (WaveMetrics, USA) to quantify the effective optical thickness ( $OT_{eff}$ ) of these NAA films by Equation 6.1:

$$OT_{eff} = 2 \cdot n_{eff} \cdot L_P \cdot \cos \theta \tag{6.1}$$

where  $OT_{eff}$  is the effective optical thickness of the NAA film (in nm),  $n_{eff}$  is its effective refractive index,  $L_P$  is its physical thickness (in nm) and q is the angle of refraction of light. Digital photographs of NAA– $\mu$ QVs were acquired by a Canon EOS 700D digital camera equipped with a Tamron 90 mm F2.8 VC USD macro mount lens under natural illumination.

# 6.2.4. Simulations of Transmission Spectra of NAA $-\mu QVs$ .

Simulated transmission spectra of NAA– $\mu$ QVs were calculated by implementing and executing a tailored transfer matrix method (TMM) algorithm in a customized MATLAB application. Experimental values of effective refractive index of each NAA stack in the structure of NAA– $\mu$ QVs and central wavelength of their characteristic resonance band were used as inputs to validate our model.  $^{36-38}$ 

## 6.2.5. Assessment of Optical Sensitivity of NAA-μQVs.

Refractive index sensitivity of hydrophilic and hydrophobic NAA– $\mu$ QVs was assessed by quantification of spectral shifts of their characteristic resonance band ( $DI_{RB}$ ) upon infiltration of their nanoporous structure with aqueous- and organic-based analytical solutions of equally varying refractive index, from  $n_{medium-low}=1.333\pm0.001$  RIU to  $n_{medium-high}=1.345\pm0.001$  RIU. Aqueous analytical solutions were prepared by dissolution of controlled concentrations of NaCl in Milli-Q water at [NaCl] = 0.00, 0.30, 0.45, 0.70, 0.90, and 1.20 M. Organic analytical solutions were prepared by mixing methanol and ethanol at volume ratios of [MeOH]:[EtOH] (v:v) = 0.80:0.20, 0.70:0.30, 0.67:0.33, 0.60:0.40, 0.50:0.50, and 0.45:0.55 to achieve a variation of  $n_{medium}$  from 1.333 to 1.345 RIU. Hydrophilic and hydrophobic NAA– $\mu$ QVs were sandwiched in a custom-built, transparent, acrylic plastic-based flow cell system, through which analytical solutions were flowed at a rate of 100  $\mu$ L min<sup>-1</sup>, using a peristaltic pump (LongerPump, Thermoline Scientific, Australia).

Real-time optical transmission spectra of hydrophilic and hydrophobic NAA– $\mu$ QVs were obtained using a transmission setup comprising a transmission stage (STAGE–RTL–T, Ocean Optics, USA) coupled to two optical fibers (QP200–2–UV–VIS, Ocean Optics, USA) connecting a tungsten light source (LS–1LL, Ocean Optics, USA) with a high-resolution optical fiber spectrometer (HDX–XR, Ocean Optics, USA). White light was focused and illuminated onto NAA– $\mu$ QVs over a circular spot size of ~2 mm in diameter and collected at their backside using a collimating lenses system (74–VIS, Ocean Optics, USA). Transmission spectra were acquired from 400 to 900 nm with an integration time of 10 ms and 20 average

measurements and processed by applying real-time Gaussian fittings to the characteristic resonance band in IgorPro (WaveMetrics, USA) to quantify  $DI_{RB}$ .

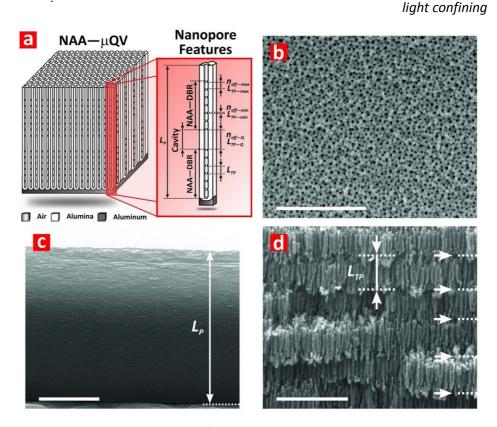
## 6.2.6. Structural Characterization of NAA-µQVs.

NAA– $\mu$ QVs and reference NAA films were characterized by field emission gun scanning electron microscopy (FEG-SEM Quanta 450, FEI, USA), and their geometric features estimated by FEG-SEM image analysis performed in ImageJ. <sup>39</sup>

#### 6.3. Results and Discussion

### 6.3.1. Structural Features of NAA-µQVs by STPA.

Figure 6.2a shows a schematic of the idealized nanoporous structure of NAA-μQVs with a graphical definition of the main geometric and optical features of these PCs. These include the total thickness  $(L_P)$ , period length at  $J_{min}$  ( $L_{TP-min}$ ) and  $J_{max}$  ( $L_{TP-max}$ ), period length ( $L_{TP} = L_{TP-min} + L_{TP-max}$ ), cavity length ( $L_{TP-Q}$ ), and effective refractive indexes at  $J_{min}$  ( $n_{eff-min}$ ),  $J_{max}$  ( $n_{eff-max}$ ), and  $J_Q$  ( $n_{eff-Q}$ ). Note that, under the design conditions used in this study,  $L_{TP-Q} = 2L_{TP-max}$  and  $n_{eff-Q} = n_{eff-max}$ . The architecture of NAA- $\mu$ QVs can be divided into three main substructures: i) two symmetric NAA-DBRs at their top and bottom featuring nanopores with modulated porosity in depth, and ii) a physical cavity layer in between them with straight cylindrical nanopores. Figure 6.2b-d depict a set of FEG-SEM images of a representative  $NAA-\mu QV_{800}$ . These NAA-based homogeneously distributed nanopores at their top surface, the average diameter of which is  $22 \pm 4$  nm (Figure 6.2b).



**Figure 6.2.** Structural engineering of NAA– $\mu$ QVs by stepwise pulse anodization (STPA). (a) Schematic showing the idealized structure of NAA- $\mu$ QVs formed by two NAA-DBRs with a physical cavity layer in between, and a graphical definition of the main geometric and optical features (NB: total thickness  $-L_P$ , nanopore length at minimum current density –  $L_{TP-min}$ , nanopore length at maximum current density –  $L_{TP-max}$ , period length –  $L_{TP} = L_{TP-min} + L_{TP-max}$ , cavity length  $-L_{TP-Q}$ , effective refractive index at minimum current density –  $n_{eff-min}$ , effective refractive index at maximum current density –  $n_{eff-max}$ , and effective refractive index at cavity current density  $-n_{eff-Q}$ ). (b) Top view FEG-SEM image of a representative NAA- $\mu$ QV<sub>800</sub> showing details of randomly distributed nanopores with an average diameter of 22 ± 4 nm (scale bar = 500 nm). (c) General cross-sectional view FEG-SEM image of a representative NAA-μQV<sub>800</sub> revealing NAA stacks with modulated porosity along their length (scale bar = 10 mm). (d) Magnified cross-sectional view FEG-SEM image of (c) showing details of nanopore modulations and period length ( $L_{TP}$ ) denoted by white dotted lines and arrows (scale bar = 500 nm) (NB: the structure of the NAA- $\mu$ QV<sub>800</sub> shown in (c) and (d) was widened by wet chemical etching in a 5 wt % aqueous solution of H<sub>3</sub>PO<sub>4</sub> at 35 °C for 6 min for imaging purposes).

The full-view cross-sectional image of the NAA– $\mu$ QV structure shown in **Figure 6.2c** reveals stacked layers of NAA, the periodicity of which is controlled by the input STPA profile. A magnified view of this structure

shows details of NAA layers stacked one over another. NAA layers feature periodically modulated porosity in depth, the period or lattice constant of which is defined as the period length ( $L_{TP}$ )—length of NAA stacks within the NAA— $\mu$ QV structure (**Figure 6.2d**).

### 6.3.2. Design of NAA-μQVs by STPA.

The optical properties of NAA– $\mu$ QVs are critically defined by the geometric and optical features of nanopores in the NAA stacks forming their structure. The Bragg condition for constructive light recirculation in a NAA– $\mu$ QV formed by two highly reflective NAA–DBRs is such that the optical thickness of each NAA stack—product of effective refractive index and physical thickness—is equal to a quarter of the resonance band central wavelength of the cavity ( $I_{RB}$ ), according to Equation 6.2<sup>26</sup>:

$$\frac{\Delta \lambda_{RB}}{4} = n_{eff-max} \cdot L_{TP-max} = n_{eff-min} \cdot L_{TP-min}$$
 (6.2)

If we reorganize terms, then we get Equations 6.3 and 6.4:

$$\frac{\Delta \lambda_{RB}}{4} = n_{eff-max} \cdot L_{TP-max} \tag{6.3}$$

$$\frac{\Delta \lambda_{RB}}{4} = n_{eff-min} \cdot L_{TP-min} \tag{6.4}$$

The period lengths at  $J_{min}$  and  $J_{max}$  (i.e.  $L_{TP-min}$  and  $L_{TP-max}$ ) can be estimated as the product between the anodic oxide growth rates (i.e.  $G_{R-min}$  and  $G_{R-max}$ ) and time durations (i.e.  $t_{min}$  and  $t_{max}$ ) at  $J_{min}$  and  $J_{max}$ , respectively. Therefore, if we substitute these expressions in Equations 6.3 and 6.4, this then gives us Equations 6.5 and 6.6:

$$\frac{\Delta \lambda_{RB}}{4} = n_{eff-max} \cdot G_{R-max} \cdot t_{max} \tag{6.5}$$

$$\frac{\Delta \lambda_{RB}}{4} = n_{eff-max} \cdot G_{R-min} \cdot t_{min} \tag{6.6}$$

Rearranging terms, then we obtain Equations 6.7 and 6.8:

$$t_{max} = \frac{\Delta \lambda_{RB}}{4} \cdot \left(\frac{1}{n_{eff-max} \cdot G_{R-max}}\right) \tag{6.7}$$

$$t_{min} = \frac{\Delta \lambda_{RB}}{4} \cdot \left(\frac{1}{n_{eff-min} \cdot G_{R-min}}\right) \tag{6.8}$$

Considering that  $T_P = t_{max} + t_{min}$  and combining Equations 6.7 and 6.8, then we get Equation 6.9:

$$T_P = \frac{\Delta \lambda_{RB}}{4} \cdot \left( \frac{1}{n_{eff-max} \cdot G_{R-max}} + \frac{1}{n_{eff-min} \cdot G_{R-min}} \right) \tag{6.9}$$

This expression provides a simple and direct means of engineering the spectral position of the resonance band of NAA– $\mu$ QVs by modifying the anodization period in the input STPA profile.A set of reference NAA films was fabricated under the same anodization conditions used in this study to determine  $G_{R-max}$ ,  $G_{R-min}$ ,  $n_{eff-max}$ , and  $n_{eff-min}$ ). The anodic oxide growth rates (i.e.,  $G_{R-min}$  and  $G_{R-max}$ ) at  $J_{min}$  and  $J_{max}$  were determined from FEG-SEM image analysis. The refractive indexes at  $J_{min}$  and  $J_{max}$  (i.e.  $n_{eff-max}$ , and  $n_{eff-min}$ ) were quantified from FFT-processed reflection spectra of these reference NAA films at  $q_{inc}$  = 15°, 25°, 35° and 45°, combining Equation 6.1 (Fabry–Pérot) and Equation 6.10 (Snell), through an iterative calculation process:

$$n_{air} \sin \theta_{Inc} = n_{eff} \sin \theta \tag{6.10}$$

where  $n_{air}$  is the refractive index of air (1.000 RIU), q is the angle of refraction, and  $q_{lnc}$  is the external angle of incidence. Values of  $G_{R-max}$ ,  $G_{R-max}$ 

 $_{min}$ ,  $n_{eff-max}$ , and  $n_{eff-min}$  under the conditions of study were measured to be 0.41  $\pm$  0.03 nm s<sup>-1</sup>, 0.09  $\pm$  0.1 nm s<sup>-1</sup>, 2.263  $\pm$  0.002 RIU, and 1.773  $\pm$  0.003 RIU, respectively. If we substitute these values in Equation 6.9, this then gives  $T_P \sim 1.84 \cdot I_{RB}$ . This expression provides a direct relationship between anodization period and position of resonance band of NAA– $\mu$ QVs.

### 6.3.3. Structural and Optical Engineering of NAA-μQVs by STPA.

A set of NAA— $\mu$ QVs featuring resonance bands across the visible spectrum was engineered by systematic variation of the anodization period in the input STPA profile, from  $T_P$  = 748 to 1496 s with  $DT_P$  = 187 s (**Table 6.1**). **Figure 6.3** shows anodization profiles, cross-sectional view FEG-SEM images, and transmission spectra of representative NAA— $\mu$ QV400, NAA— $\mu$ QV600, and NAA— $\mu$ QV800, while (**Figure 6.4**) compiles these details for all NAA— $\mu$ QVs assessed in this study (i.e., NAA— $\mu$ QV400—NAA— $\mu$ QV800). A qualitative analysis of full-view anodization profiles shown in **Figures 6.3a—c** reveals that a stepwise pulsed input current density profile, with an amplitude of  $A_J = J_{max} - J_{min} = 0.840$  mA cm<sup>-2</sup>, results in a pulsed output voltage profile with an average amplitude of ~12.5 V and a frequency that follows closely that of the input current density waveform.

Magnified views of these anodization profiles show an electrochemical output in the form of asymmetric voltage pulses featuring capacitor-like charge-discharge regions, which correspond to the sections at  $J_{max}$  and  $J_{min}$  of the input STPA pulses, respectively. This electrochemical response is associated with the hemispherical barrier oxide layer closing the tip of NAA's nanopores at the anodic oxide growth front (i.e., interface anodic oxide–metal).<sup>40,41</sup>

ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla light confining

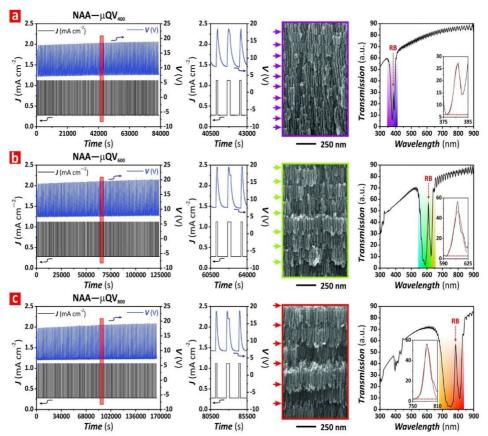
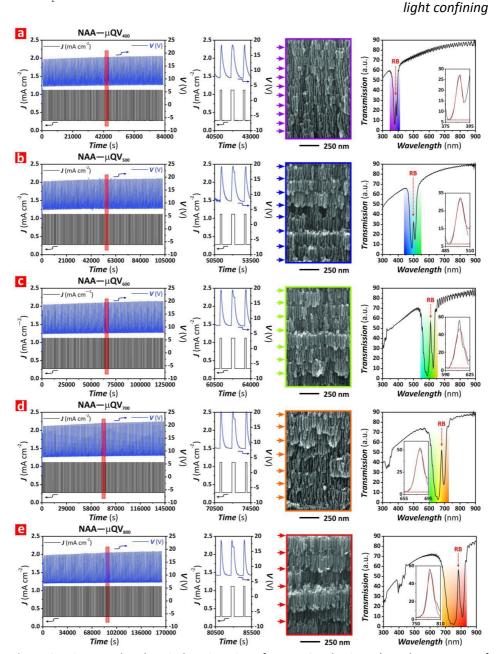


Figure 6.3. Structural and optical engineering of NAA- $\mu$ QVs by STPA (NB: the structure of NAA- $\mu$ QVs shown in these FEG-SEM images was widened by wet chemical etching in a 5 wt % aqueous solution of H<sub>3</sub>PO<sub>4</sub> at 35 °C for 6 min for imaging purposes). (a) Full-view of anodization profile used to fabricate NAA- $\mu$ QV<sub>400</sub> with a magnified view of red rectangle showing details of the input current density and output voltage response (left), magnified cross-sectional view FEG-SEM image of a representative NAA- $\mu$ QV<sub>400</sub> with purple arrows indicating the period length (center), and full-view transmission spectrum of a NAA- $\mu$ QV<sub>400</sub> with details of the RB (inset) (right). (b) Full-view of anodization profile used to fabricate NAA- $\mu$ QV<sub>600</sub> with a magnified view of red rectangle showing details of the input current density and output voltage response (left), magnified cross-sectional view FEG-SEM image of a representative NAA- $\mu$ QV<sub>600</sub> with green arrows indicating the period length (center), and full-view transmission spectrum of a NAA- $\mu$ QV<sub>600</sub> with details of the RB (inset) (right). (c) Full-view of anodization profile used to fabricate NAA- $\mu$ QV<sub>800</sub> with a magnified view of red rectangle showing details of the input current density and output voltage response (left), magnified cross-sectional view FEG-SEM image of a representative NAA- $\mu$ QV<sub>800</sub> with red arrows indicating the period length (center), and full-view transmission spectrum of a NAA- $\mu$ QV<sub>800</sub> with details of the RB (inset) (right).

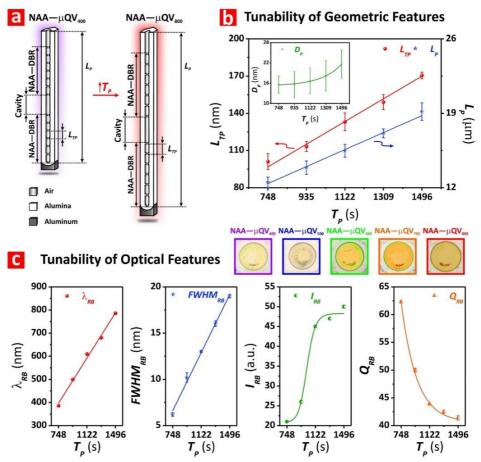
Anodic aluminum oxide is an electrical insulator that delays the flow of electrons and ionic species (i.e.,  $AI^{3+}$ ,  $O^{2-}$ , and  $OH^-$ ) driven by the applied electric field across the barrier oxide layer during anodization. Dynamic change in input current density, results in an adjustment of the barrier oxide layer thickness to counterbalance the induced change in electric field. Analysis of anodization profiles reveals a short time delay (~10–18 s) between change in input current density and output voltage response for all NAA– $\mu$ QVs developed in this study (**Figure 6.4**). This indicates that these anodization conditions make it possible to precisely engineer nanopore morphology modulations in depth by judicious modification of the input current density.

FEG-SEM cross-sectional analysis of representative NAA– $\mu$ QV<sub>400</sub>, NAA– $\mu$ QV<sub>600</sub>, and NAA– $\mu$ QV<sub>800</sub> films upon mechanical fracture reveals a layered structure of NAA stacks featuring periodically modulated porosity along their length (**Figures 6.3a–c**). The structural periodicity or lattice constant of these 1D NAA– $\mu$ QVs is defined as the period length ( $L_{TP}$ )—thickness of NAA stacks within the NAA– $\mu$ QV structure. It is apparent from color arrows in **Figures 6.3a–c** and **Figure 6.4** that  $L_{TP}$  increases with anodization period in the input STPA pulses. Optical transmission spectra of NAA– $\mu$ QVs shown in **Figures 6.3a–c** and **Figure 6.4** is characterized by an intense, broad photonic stopband (PSB), the features of which are determined by the two NAA–DBRs forming this PC structure. Magnified views of these PBSs reveal well-resolved, narrow resonance bands (RBs) at approximately their center. This optical feature is attributable to constructive light recirculation within NAA– $\mu$ QVs, which results from the intercalation of a physical cavity layer between the two NAA–DBRs.



**Figure 6.4.** Structural and optical engineering of NAA–μQVs by STPA (NB: the structure of NAA–μQVs shown in these FEG-SEM images was widened by wet chemical etching in a 5 wt % aqueous solution of  $H_3PO_4$  at 35°C for 6 min for imaging purposes). (a–e) Full-view of anodization profile used to fabricate NAA–μQV<sub>400</sub>—NAA–μQV<sub>800</sub> with a magnified view of red rectangle showing details of the input current density and output voltage response (left), magnified cross-sectional view FEG-SEM image of a representative NAA–μQV<sub>400</sub>—NAA–μQV800 with color arrows indicating the period length (center), and full-view transmission spectrum of NAA–μQV<sub>400</sub>—NAA–μQV<sub>800</sub> with details of RBs (inset) (right).

It is also apparent from these graphs that RB red-shifts (shift toward longer wavelengths) its position with increasing anodization period. Note that the resonance band spectral position is determined by the intrinsic relationship between the geometric and optical properties of the cavity layer and the NAA stacks forming the structure of NAA-DBRs, which is designed to fulfil the conditions  $L_{TP-Q} = 2 \cdot L_{TP-max}$  and  $n_{eff-Q} = n_{eff-max}$ . An increment in  $T_P$  in the input current density results in longer  $L_{TP}$  and  $L_{TP-Q}$ within the NAA-DBRs and the cavity layer composing the PC structure, respectively (Figure 6.5a). As such, the resonance band position ( $I_{RB}$ ) can be precisely engineered across the broad spectrum by modification of  $T_P$ in the input STPA profile. Figure 6.5b shows the intrinsic dependence of the total thickness ( $L_P$ ) and period length ( $L_{TP}$ ) in NAA- $\mu$ QVs with  $T_P$ , from 748 to 1496 s. It is apparent from this graph that both  $L_P$  and  $L_{TP}$  increase linearly with increasing  $T_P$  at rates of 8.6  $\pm$  3.4 and 0.10  $\pm$  0.01 nm s<sup>-1</sup>, respectively. Figure 6.5b (inset) shows the dependence of nanopore diameter at the top of NAA- $\mu$ QVs ( $D_P$ ) with the anodization period, where this geometric parameter increases exponentially with  $T_P$  according to the expression  $D_P$  (nm) = 15 + 0.06·Exp[ $(T_P(s) - 373)/241$ ]. This finding is reasonable since the longer  $T_P$  the more time the NAA- $\mu$ QV structure is exposed to the acid electrolyte, which inevitably leads to progressive etching of its structure. Figure 6.5c summarizes the dependence of the optical features of the characteristic resonance band of NAA-µQVs with  $T_P$ . It is apparent that  $\lambda_{RB}$  red-shifts its position linearly with increasing  $T_P$ at a rate of  $0.52 \pm 0.01$  nm s<sup>-1</sup>. For instance,  $I_{RB}$  shifts its position from 386  $\pm$  1 nm at  $T_P$  = 748 nm to 786  $\pm$  1 nm at  $T_P$  = 1496 s, which correspond to NAA- $\mu$ QV<sub>400</sub> and NAA- $\mu$ QV<sub>800</sub>, respectively.



**Figure 6.5** Tunability of structural and optical features of NAA–μQVs by modification of anodization period in the input STPA profile. (a) Schematics of idealized nanopores of NAA–μQVs produced at distinct anodization periods ( $T_P$ ) showing details of the effect of this fabrication parameter on the structural features of these NAA-based PCs. (b) Dependence of total thickness ( $L_P$ ), period length ( $L_{TP}$ ), and nanopore diameter ( $D_P$ ) with anodization period, from  $T_P$  = 748 to 1496 s with  $DT_P$  = 187 s, for NAA–μQV<sub>400</sub>—NAA–μQV<sub>800</sub>. (c) Dependence of central wavelength position ( $I_{RB}$ ), full width at half maximum (FWHM<sub>RB</sub>), intensity ( $I_{RB}$ ), and quality factor ( $I_{RB}$ ) with anodization period, from  $I_P$  = 748 to 1496 s with  $I_P$  = 187 s, for NAA–μQV<sub>400</sub>—NAA–μQV<sub>800</sub>, with inset showing digital pictures of these NAA–PCs featuring interferometric colors (NB: the diameter of NAA–μQVs was ~1 cm).

Comparative analysis between measured and calculated values of  $I_{RB}$  using **Equation 6.9** reveals a residual deviation that oscillates between 0.1 and 5 %, which demonstrates the suitability of our model to tune the position of the resonance band of NAA– $\mu$ QVs by the input anodization period in the STPA profile.

To further validate the model, a custom-built MATLAB application using the TMM approach was used generate simulated optical spectra of NAA– $\mu$ QVs, using experimentally quantified values of  $n_{eff-max}$ ,  $n_{eff-min}$ , and  $l_{RB}$  as inputs. <sup>36–38</sup> However, an analysis of simulated and experimentally estimated values of  $L_{TP-max}$  and  $L_{TP-min}$  for NAA- $\mu$ QV<sub>400</sub>-NAA- $\mu$ QV<sub>800</sub> shown in **Table 6.2** reveals a minimum deviation of ~0.1–5 %.

**Table 6.2.** Comparison between experimental and simulated values of period length at  $J_{min}$  ( $LTP_{min}$ ) and Jmax ( $LTP_{max}$ ).

	Experimental <sup>†</sup>		Simu	ılated <sup>‡</sup>	Deviation*		
NAA-μQV	<i>LTP<sub>min</sub></i> (nm)	LTP <sub>max</sub> (nm)	<i>LTP<sub>min</sub></i> (nm)	<i>LTP<sub>max</sub></i> (nm)	LTP <sub>min</sub> (%)	<i>LTP<sub>max</sub></i> (%)	
NAA- μQV400	44	58	42	54	5.4	5.7	
NAA- μQV500	55	72	54	71	2.2	2.2	
NAA- μQV600	66	87	66	86	0.1	0.7	
NAA- μQV700	77	101	73	96	4.7	5.1	
NAA- μQV800	88	115	84	111	3.7	4.0	

<sup>+</sup>Values estimated as LTP-min =  $tmin \cdot GR$ -min and LTP-max =  $tmax \cdot GR$ -max

<sup>‡</sup>Values estimated from simulations

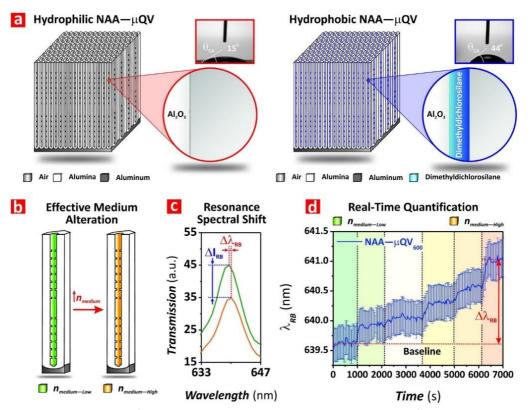
<sup>\*</sup>Values estimated as:

This demonstrates that our model can mechanistically describe the optical properties of these NAA-based PCs with precision, providing a useful tool to design NAA-µQVs with well-resolved resonance bands across the visible spectrum by modification of the input anodization period. It is also apparent that the width of the resonance band (FWHM<sub>RB</sub>) increases linearly with increasing  $T_P$  at a rate of 0.017  $\pm$  0.001 nm s<sup>-1</sup>. FWHM<sub>RB</sub> increases from 6.2  $\pm$  0.2 nm for NAA- $\mu$ QV<sub>400</sub> to 19.0  $\pm$  0.3 nm for NAA- $\mu QV_{800}$ . This analysis also indicates that the intensity of the resonance band  $(I_{RB})$  increases with increasing  $T_P$  following a sigmoidal trend. It is worthwhile noting that an interesting characteristic of NAA-μQVs is their interferometric color, which results from efficient light reflection forbidden light—at those visible spectral regions where their characteristic PSB and RB are located. Digital images of NAA-µQVs shown in **Figure 6.5c** reveal that, while NAA- $\mu$ QV<sub>400</sub> and NAA- $\mu$ QV<sub>500</sub> are transparent, their analogues produced at longer  $T_P$  feature vivid interferometric colors (i.e., green for NAA-μQV<sub>600</sub>, orange for NAA- $\mu QV_{700}$ , and red for NAA- $\mu QV_{800}$ ). This result is attributable to the highest  $I_{RB}$  values achieved by these NAA- $\mu$ QVs, which were found to be 45 ± 1, 47 ± 1, and 50 ± 1 a.u., respectively. The quality factor  $(Q_{RB})$ —ratio of  $I_{RB}$ to FWHM<sub>RB</sub>— is parameter that quantifies how good a given optical microcavity confines light within its structure. Figure 6.5c demonstrates that  $Q_{RB}$  decreases exponentially  $T_P$  according to the expression  $Q_{RB} = 41$ + 865·Exp[ $-T_P$  (s)/203]. For instance,  $Q_{RB}$  for NAA- $\mu$ QV<sub>400</sub> and NAA- $\mu QV_{800}$  are estimated to be 62.3  $\pm$  0.2 and 41.4  $\pm$  0.4, respectively. Decrease in  $Q_{RB}$  with  $T_P$  is attributable to the progressive etching of the nanoporous structure with increasing anodization time. At a fixed number of STPA pulses, NAA-μQVs produced with longer anodization period are

exposed to the acid electrolyte for longer time. Extended anodization time results in increased light scattering and an unbalanced distribution of effective optical thickness between NAA stacks at the top and bottom of the NAA– $\mu$ QVs due to extensive and progressive chemical etching. As such, quality of light confinement within these NAA–PCs is worsened with anodization time. This observation will be addressed elsewhere by a new methodology to enhance controllability of  $Q_{RB}$  with anodization time.

# 6.3.4. Surface Chemistry Engineering and Sensing Principle of NAA- $\mu$ QVs.

As-produced NAA is an amorphous, hydrophilic, amphoteric metal oxide that features an onion-like chemical composition with concentrically decreasing concentration of acid electrolyte-incorporated impurities, from the outer nanopore wall or inner surface—surface exposed to acid electrolyte—to the inner cell boundary formed of pure Al<sub>2</sub>O<sub>3</sub>. 44,45 The inner surface of NAA is rich in Al3+ and O2- vacancies, and OH- groups, which enable facile anchoring of functional molecules to tailor NAA-based PCs for selective optical sensing purposes.<sup>22</sup> The hydrophilic or hydrophobic character of the surface of a solid-state sensing platform can dramatically determine its sensing performance. As such, understanding the role of wettability on the sensitivity of NAA-µQVs is a critical step to enabling this technology for real-life sensing applications. With this in mind, we engineered two types of NAA-µQVs with spectrally tunable resonance bands across the visible spectrum: i) as-produced or 'hydrophilic' NAA-µQVs, and ii) dichlorodimethysilane-functionalized or 'hydrophobic' NAA-μQVs (**Figure 6.6a**). It is worthwhile nothing that, in the context of this study, the terms 'hydrophilic' and 'hydrophobic' do not refer to the conventional contact angle classification of 90°. Contact angle (CA) measurements in hydrophilic and hydrophobic NAA– $\mu$ QVs (**Figure 6.6a** insets) indicate an increasing CA upon surface chemistry functionalization, from ~15 to 44°, for as-produced and dichlorodimethysilane-functionalized NAA– $\mu$ QVs, respectively.



**Figure 6.6.** Chemical functionalization and optical sensing principle of NAA– $\mu$ QVs fabricated by STPA. (a) Schematics showing the idealized structure of as-produced ('hydrophilic') and dichlorodimethysilane-functionalized ('hydrophobic') NAA– $\mu$ QVs with insets displaying contact angle (CA) measurements of ~15 and 44°, respectively. (b) Schematic showing details of the nanoporous structure of NAA– $\mu$ QVs upon infiltration with solutions of varying refractive index. (c) Optical transmission spectra of a representative NAA– $\mu$ QV600 showing details of its resonance band in the baseline solution ( $n_{medium}$  = 1.333 RIU, green line) and in the analytical solution with highest refractive index ( $n_{medium}$  = 1.345 RIU, orange line), including a graphical description of  $l_{RB}$  shift ( $Dl_{RB}$ ) and  $l_{RB}$  decay ( $Dl_{RB}$ ). (d) Real-time monitoring of resonance band shift with increasing  $n_{medium}$ , from  $n_{medium-low}$  = 1.333 RIU to  $n_{medium-high}$  = 1.345 RIU, for a representative NAA– $\mu$ QV600.

light confining

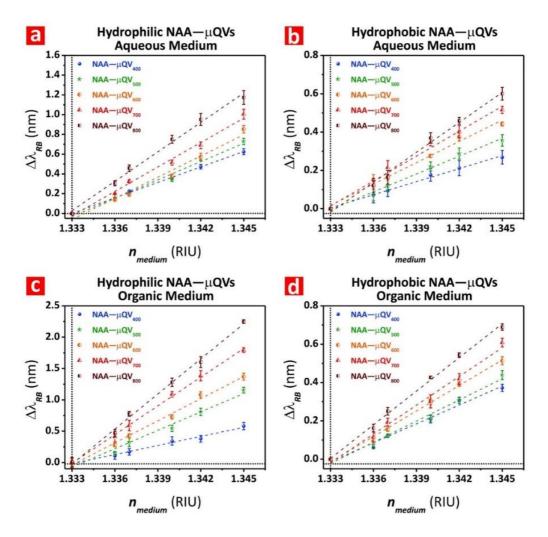
Incoming electromagnetic waves of specific wavelengths are confined with the structure of NAA– $\mu$ QVs by resonant, constructive recirculation. As such, any perturbation of the effective medium of these nanoporous PCs alters the properties of confined light—core sensing principle (**Figure 6.6b**). **Figure 6.6c** shows an example of how changes in refractive index of the medium filling the nanopores of NAA– $\mu$ QVs lead to quantifiable shifts in position ( $DI_{RB}$ ) and decays in intensity ( $DI_{RB}$ ) of their characteristic resonance band. Proportionality between induced perturbation and optical response makes NAA– $\mu$ QVs a suitable class of optical sensing transducer platforms for sensing applications.

**Figure 6.6d** demonstrates how dynamic alterations of the effective medium of NAA– $\mu$ QVs by infiltration of their nanoporous structure with media of increasing refractive index ( $n_{medium}$ ) are translated into real-time, quantifiable shifts in  $I_{RB}$ , where this optical feature red-shifts its position with increasing  $n_{medium}$ , from  $n_{medium-low} = 1.333$  RIU to  $n_{medium-low} = 1.345$  RIU. Prior to injection of aqueous- and organic-based analytical solutions of equally varying refractive index (i.e., from 1.333 to 1.345 RIU) into the flow cell system, a stable baseline is obtained in the corresponding reference solution (i.e.,  $n_{medium} = 1.333$  RIU) for ~15 min.

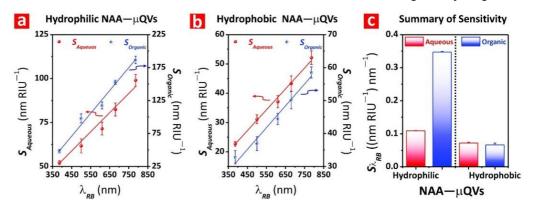
Increasing the refractive index of the medium filling the nanoporous structure of NAA– $\mu$ QVs by injecting analytical solutions of increasing  $n_{medium}$  into the flow cell results in an almost instantaneous red shift to  $l_{RB}$ . Spectral shifts of NAA– $\mu$ QVs' RB are found to be proportional to the increment in  $n_{medium}$ .

## 6.3.5. Effect of Surface Chemistry and Resonance Band Features on Sensitivity of NAA-µQVs.

To elucidate the combined effect of spectral resonance position and surface chemistry on the sensitivity of NAA-µQVs, quantification and comparison of sensing performance indicators (i.e., sensitivity – S and linearity –  $R^2$ ) was performed using  $DI_{RB}$  as a reference sensing parameter. Figure 6.7 summarizes spectral shifts in resonance band position for hydrophilic and hydrophobic NAA- $\mu$ QVs upon variation of  $n_{medium}$  in aqueous- and organic-based analytical solutions. It is apparent from these results that sensitivity of both hydrophilic and hydrophobic NAA-µQVs, defined as the slope of linear fittings shown in **Figures 6.8a–d**, increases with  $I_{RB}$ , in both organic and aqueous analytical solutions. Linear trends indicate a strong proportionality between effective medium perturbation and optical response in NAA-µQVs. Table 6.3 summarizes the sensing performance parameters obtained from linear fittings shown in Figure **6.8**. These results indicate that hydrophilic NAA–μQV<sub>800</sub> in organic-based solutions, are the most sensitive structure under the conditions of study. These achieve a sensitivity of 186.5 ± 5.6 nm RIU<sup>-1</sup> and a linearity of 0.9955. Further qualitative analysis of these fittings also indicates that hydrophilic NAA-µQVs are more sensitive than their hydrophobic counterparts, in both aqueous and organic media. Figure 6.8 provides a comprehensive summary of the sensitivity of hydrophilic and hydrophobic NAA- $\mu$ QVs in aqueous and organic media as a function of  $I_{RB}$ . Figures 6.8a and b demonstrate that sensitivity of hydrophilic and hydrophobic NAAµQVs toward changes in refractive index of the medium filling the nanopores increases linearly with  $I_{RB}$ . However, the optical response of these optical transducers varies significantly with surface chemistry and nature of the medium filling the nanopores for a specific range of  $n_{medium}$ . Figure 6.8c summarizes values of sensitivity per unit of resonance band position, defined as  $S_{IRB} = S/I_{RB}$ .



**Figure 6.7.** Assessment of sensing performance of hydrophilic and hydrophobic NAA– $\mu$ QVs with tunable resonance bands upon exposure to aqueous- and organic-based analytical solutions of varying refractive index ( $n_{medium}$  = 1.333–1.345 RIU) using spectral shifts in their characteristic resonance band ( $Dl_{RB}$ ) as a core sensing principle. (a) Sensing performance of hydrophilic NAA– $\mu$ QV<sub>400</sub>—NAA– $\mu$ QV<sub>800</sub> in aqueous medium. (b) Sensing performance of hydrophobic NAA– $\mu$ QV<sub>400</sub>—NAA– $\mu$ QV<sub>800</sub> in organic medium. (c) Sensing performance of hydrophobic NAA– $\mu$ QV<sub>400</sub>—NAA– $\mu$ QV<sub>800</sub> in organic medium. (d) Sensing performance of hydrophobic NAA– $\mu$ QV<sub>400</sub>—NAA– $\mu$ QV<sub>800</sub> in organic medium.



**Figure 6.8.** Optical sensitivity of hydrophilic and hydrophobic NAA– $\mu$ QVs with tunable resonance band across the visible spectrum in aqueous- ( $S_{Aqueous}$ ) and organic-based ( $S_{Organic}$ ) solutions. (a) Optical sensitivity of hydrophilic NAA– $\mu$ QVs in aqueous solutions as a function of  $I_{RB}$ . (b) Optical sensitivity of hydrophilic NAA– $\mu$ QVs in organic solutions as a function of  $I_{RB}$ . (c) Summary of sensitivity per unit of resonance band position ( $S_{IRB}$ ) for hydrophilic and hydrophobic NAA– $\mu$ QVs.

Hydrophilic NAA–μQVs are clearly more sensitive than their hydrophobic analogues, in both aqueous- and organic-based solutions, with SIRB values of 0.109  $\pm$  0.001 and 0.347  $\pm$  0.002 (nm RIU<sup>-1</sup>) nm<sup>-1</sup>, respectively. Hydrophilic NAA-μQVs are found to be more than three-fold more sensitive to changes in refractive index when sensing is performed in organic-based liquid matrices. Conversely, hydrophobic NAA-µQVs are found to be slightly more sensitive to alterations of refractive index in aqueous medium, with sensitivities of  $0.072 \pm 0.002$  and  $0.066 \pm 0.006$ (nm RIU<sup>-1</sup>) nm<sup>-1</sup> in aqueous- and organic-based media, respectively. Sensitivity of NAA-based PCs relies on i) size of analyte molecules, ii) degree to which analyte molecules increase the refractive index of the medium filling the nanopores, iii) molecule-to-surface interaction strength, and iv) spectral position and quality of light confinement. Previous studies on porous silicon-based PCs have pointed that optical sensitivity of these optical structures is inversely and directly proportional to the  $FWHM_{RB}$  and  $Q_{RB}$ , respectively, where PCs featuring narrower and

higher quality bands provide more sensing resolution upon modification of their effective medium. 46 Conversely, sensitivity of NAA–μQVs toward changes in n<sub>medium</sub> is found to increase with increasing FWHM<sub>RB</sub> and decreasing QRB. As such, it is necessary to consider other contributing factors that might play a more significant role than that of FWHM<sub>RB</sub> and Q<sub>RB</sub> in determining the sensitivity of this type of nanoporous PCs. Aqueous solutions of NaCl contain Na<sup>+</sup> and Cl<sup>-</sup> ions, and H<sub>2</sub>O molecules, while organic analytical mixtures used in this study are composed of MeOH and EtOH molecules. The size of these molecules and ions (< 1 nm) is much smaller than the visible light wavelength. Therefore, it is possible to assume that the size of analyte molecules does not contribute to the differences in sensitivity observed in hydrophilic and hydrophobic NAAμQVs. Values of refractive index for both aqueous- and organic based analytical solutions used in this study were the same (i.e.,  $n_{medium} = 1.333$ , 1.336, 1.337, 1.340, 1.342, and 1.345 RIU). Analysis of optical absorbance of these solutions from 400 to 800 nm indicates that both NaCl and MeOH-EtOH solutions absorb more light at higher wavelengths within a comparable range of absorbance (~0.40-0.42 a.u.) As such, increasing sensitivity per unit of resonance band position in hydrophilic and hydrophobic NAA-µQVs for both aqueous- and organic-based solutions can be attributed to increasing optical absorbance of analytical solutions with wavelength, where this parameter is found to be more critical than that of FWHM<sub>RB</sub> and Q<sub>RB</sub> in determining the sensitivity of NAA-µQVs under the conditions of study. Analysis of SIRB also reveals that, while sensitivity in hydrophobic NAA-μQVs is statistically the same in aqueous and organic media (i.e.,  $0.072 \pm 0.002$  and  $0.066 \pm 0.006$  (nm RIU<sup>-1</sup>) nm<sup>-1</sup>, respectively), hydrophilic NAA-µQVs show considerable variation in sensitivity with media, where  $S_{IRB}$  is higher when changes in  $n_{medium}$  are induced by an organic medium (i.e.,  $0.109 \pm 0.001$  and  $0.347 \pm 0.002$  (nm RIU<sup>-1</sup>) nm<sup>-1</sup> for aqueous and organic solutions, respectively). Ghazzal et al. developed opal-like  $SiO_2$ – $TiO_2$  PCs with tunable hydrophilic–hydrophobic balance to investigate the effect of this parameter on optical sensitivity upon infiltration with water and hexane.<sup>47</sup> These opal PCs showed decreasing and increasing sensitivity toward water and hexane with increasing hydrophobic character, respectively.

**Table 6.3.** Summary of optical sensing performance parameters (sensitivity — S and linearity — R2) for hydrophilic and hydrophobic NAA- $\mu$ QVs in aqueous- and organic-based analytical solutions of varying refractive index.

NAA–μQV	Surface Chemistry	Medium	S (nm RIU <sup>-1</sup> )	R <sup>2</sup>	
NAA-μQV400		Aqueous	52.2 ± 1.1	0.9991	
NAA-μQV500	Hydrophilic		61.7 ± 4.3	0.9764	
NAA-μQV600			71.5 ± 5.6	0.9697	
NAA-μQV700			82.4 ± 3.7	0.9901	
NAA-μQV800			99.3 ± 4.0	0.9920	
NAA-μQV400		Organic	48.2 ± 2.8	0.9834	
NAA-μQV500			97.9 ± 6.8	0.9763	
NAA-μQV600	Hydrophilic		117.5 ± 5.0	0.9909	
NAA-μQV700			152.6 ± 3.1	0.9979	
NAA-μQV800			186.5 ± 5.6	0.9955	
NAA-μQV400		Aqueous	22.7 ± 0.8	0.9934	
NAA-μQV500			31.1 ± 1.3	0.9909	
NAA-μQV600	Hydrophobic		37.1 ± 2.1	0.9841	
NAA-μQV700			43.3 ± 2.6	0.9828	
NAA-μQV800			52.1 ± 2.2	0.9908	
NAA-μQV400	Hydrophobic	Organic	32.8 ± 2.0	0.9816	
NAA-μQV500			38.9 ± 2.1	0.9845	
NAA-μQV600			44.4 ± 1.7	0.9929	
NAA-μQV700			50.1 ± 2.6	0.9869	
NAA-μQV800			58.5 ± 1.7	0.9959	

light confining

However, it is worth noting that these nanoporous PCs featured a  $^{\sim}5-7$  times smaller diameter ( $^{\sim}3-6$  nm) than that of NAA $-\mu$ QVs. As such, these PCs are more susceptible to infiltration constraints due to flow retention of water and hexane molecules when these solutions flow through hydrophilic and hydrophobic nanopores. **Figure 6.5d** reveals a fast, almost instantaneous rise in DI<sub>RB</sub> upon exchange of analytical solution flowing through the flow cell system, in both aqueous and organic solutions. This suggests that no flow constraints occur within NAA $-\mu$ QVs under the conditions of study. Some et al. studied the effect of wettability on the optical sensitivity of hydrophilic graphene and hydrophobic reduced graphene oxide layers. <sup>48</sup> Hydrophilic graphene showed higher sensitivity to volatile organic compounds that its hydrophobic counterpart.

Differences in sensitivity were attributed to the presence of polar functional groups on the surface of hydrophilic graphene, which increase the strength of molecule-to-surface interactions between organics and graphene. We hypothesize that sensitivity differences between hydrophilic and hydrophobic NAA– $\mu$ QVs in aqueous and organic analytical solutions are critically determined by molecule-to-surface interactions. The surface of as-produced NAA– $\mu$ QVs features aluminum and oxygen vacancies, and hydroxyl groups. These charged functionalities would favor polar interactions with organics, enhancing the overall sensitivity of the PC structure. Upon functionalization with dichlorodimethylsilane, the inner surface of NAA– $\mu$ QVs is homogeneously coated with a layer of Cl groups, which would minimize the strength of molecule-to-surface interactions and homogenize the optical response of the nanoporous PC structure upon infiltration with aqueous and organic solutions. To conclude, analysis of the overall sensitivity of NAA– $\mu$ QVs demonstrates

that the performance of these light-confining nanoporous photonic crystal structures is comparable to that of other nanoporous microcavity structures produced by anodization. <sup>25,26,28</sup> Although emerging high-Q plasmonic resonance structures can provide much higher sensitivities (one order of magnitude superior ~1,000 nm RIU $^{-1}$ ) $^{49,50}$ , NAA $^{-}\mu$ QVs could open exciting new opportunities to further enhance these performances through hybrid composite structures, harnessing phenomena such as Tamm plasmon resonance.

#### 6.4. Conclusion

In summary, we have determined for the first time the combined effect of spectral light confinement features and surface chemistry on optical sensitivity using nanoporous anodic alumina optical microcavities as model light-confining photonic crystal structures. The nanoporous architecture of NAA-µQVs featuring two distributed Bragg mirrors with a physical cavity layer in between was engineered by stepwise pulse anodization. Model NAA-µQVs showed well-resolved, spectrally tunable resonance bands ~400 to 800 nm by judicious modification of the anodization period in the input STPA profile. A theoretical model for precise engineering of NAA-µQVs' resonance band across the visible spectrum was developed. Comparison between simulated and experimental optical transmission spectra demonstrated that our model can accurately predict the optical properties of these NAA-based PC structures, using experimental values of effective refractive index and anodic oxide growth rate. Optical sensitivity of as-produced (hydrophilic) and dichlorodimethylsilane-functionalized (hydrophobic) NAA-μQVs was assessed by analyzing dynamic spectral shifts of NAA– $\mu$ QVs' resonance band upon infiltration with organic- and aqueous-based analytical solutions of equally varying refractive index, from 1.333 to 1.345 RIU. The findings demonstrated that optical sensitivity of both hydrophilic and hydrophobic NAA– $\mu$ QVs increases linearly with the position of their characteristic resonance, in both organic and aqueous solutions, due to increasing optical absorbance.

Analysis of sensitivity also revealed that hydrophilic NAA– $\mu$ QVs show ~81 and 35 % superior sensitivity to their hydrophobic counterparts for organic- and aqueous-based analytical solutions, respectively. We hypothesize that homogeneity in sensitivity of hydrophobic NAA– $\mu$ QVs in organic and aqueous solutions was attributable to stabilization by Cl groups deposited onto the inner surface of these nanoporous PCs. In contrast, the presence of charged functionalities on the surface of hydrophilic NAA– $\mu$ QVs enables strong molecule-to-surface interactions that enhance sensitivity toward organic- and aqueous-based solutions of varying refractive index. In this chapter we present a new avenue to explore the unique light-confining properties of NAA-based PC structures for optical sensing applications. Precise design and engineering of structural, optical, and chemical properties of these PCs provide exciting new opportunities to harness distinct forms of light–matter interactions for a broad range of photonic technologies and sensing applications.

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UNIVERSITAT ROVIRA I VIRGILI

ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla

Chapter 7. Tuning Intrinsic

Photoluminescence of

Multispectral Nanoporous

Anodic Alumina Photonic

Structures

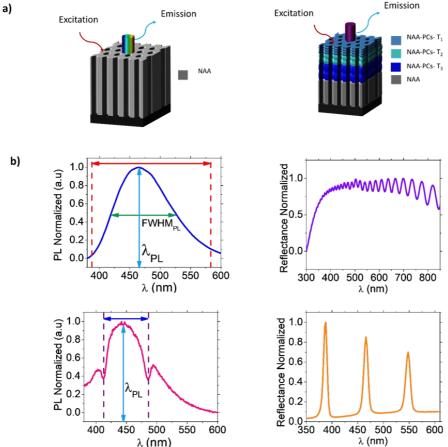
UNIVERSITAT ROVIRA I VIRGILI ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla In this chapter, the precise structural engineering and tuning of intrinsic photoluminescence emissions from nanoporous anodic alumina photonic crystals (NAA–PCs) is demonstrated. A smart structural design by a combination of pulse and constant anodization in distinct acid electrolytes makes it possible to engineer a novel heterogenous optical structure consisting of a non-emitting, light-filtering layer in the form of multispectral NAA–PC, and an intrinsically light-emitting layer of NAA. MS–NAA–PCs are engineered to feature three intense, well-resolved photonic stopbands, the position of which are spaced across the visible spectrum, from ~380 to 560 nm. These advances pave the way for novel designs of intrinsic, light-emitting NAA-based photonic crystals structures, which could find broad applicability across light technologies such as sensing and biosensing, photodetection, and solar light harvesting.

### 7.1 Introduction.

Solid-state light-driven luminescence - henceforth "photoluminescence" or PL — is a class of light—matter interaction in which incident photons absorbed by a material's atoms excite electrons to higher energy levels. Once excited, electrons undergo certain relaxation processes, through which photons are re-radiated or emitted in the form of a light beam. The properties of the emitted photoluminescent beam rely on the electronic band structure of the photo-excited material. Characteristically, PL emissions from solid-state materials with defects in their electronic band structure are spectrally broad, featuring a Gaussian-like emission centered within the vicinity of the exciton resonance — typically at a longer wavelength than that of excitation. Broad PL emissions can be narrowed by distinct strategies to fulfil requirements for specific

applications such as lasing<sup>4</sup>, LEDs<sup>5-6</sup>, bioimaging<sup>7</sup>, and diagnostics and sensing<sup>8-9</sup>. Of all these, engineering the structure of light-emitting materials at the nanoscale in the form of photonic crystals (PCs) enables highly directional emission of light with tunable wavelength by confining, enhancing, and attenuating emitted light at specific, narrow spectral regions<sup>10-11</sup>. PCs are optical structures with allowed and forbidden photonic stopbands that modify the group velocity of incident or emitted photons when these flow through the PCs' structure. Light-matter interactions in PCs can be tuned with precision by engineering their architecture so that regions with high and low refractive indexes are periodically and spatially distributed following specific patterns. 12 A variety of PC forms based on a broad range of materials can be produced to control electromagnetic waves with versatility over the broad spectrum, from UV to IR. Currently, PCs have multiple applications including chemical sensing and biosensing<sup>13-18</sup>, photonic encoding<sup>19</sup>, lasing<sup>20-25</sup>, and photocatalysis<sup>26-27</sup>. Nanoporous PCs are particularly suitable platform materials to tailor photo-induced light emissions, both extrinsically and intrinsically. In the former mode, a host nonphotoluminescent nanoporous PC is infiltrated with a photoluminescent material to enhance, filter or guide its light emission<sup>27</sup>, while in the latter configuration a photoluminescent nanoporous PC material filters its own PL emission<sup>28</sup>. Nanoporous anodic alumina (NAA) has long been devised as an ideal nanoporous PC platform material due to its cylindrical nanopores with well-defined and highly controllable geometric features.<sup>29-32</sup> NAA is produced by electrochemical oxidation anodization — of aluminum, which is a cost-effective and fully scalable top-down industrial process compatible with conventional micro- and nanofabrication. While architecture, dimensions and distribution of nanopores in NAA can be precisely engineered in a variety of NAA-based PCs (NAA-PCs) during anodization<sup>33-35</sup>, its intrinsic optical properties refractive index and photoluminescence — are critically determined by the anodizing acid electrolyte, anodization regime, and post-anodization treatments such as annealing<sup>36</sup>. Origin of PL in NAA is thought to be attributable to two types of photoluminescent centers: (i) F+ centers<sup>37-39</sup> related to ionized oxygen vacancies, and (ii) F- centers associated with carboxylate impurities incorporated from the acid electrolyte during anodization<sup>40-41</sup>. Position and intensity of NAA's PL emission depend intrinsically on the quantity of F+ and F- centers. NAA films produced in oxalic acid feature more intense PL emission than that of its counterparts fabricated in sulfuric or phosphoric acids<sup>42-46</sup>. NAA's PL intensity also decreases with annealing temperature due to elimination of oxygen vacancies and impurities in its structure through crystallographic organization and burning under oxygen atmosphere. 47-52 Pioneering studies on 2D NAA-PCs featuring straight nanopores demonstrated their application as host materials to tune PL emissions from fluorescent dyes infiltrated in their nanoporous matrix. In this system, the red edge of the characteristic photonic stopband (PSB) of NAA-PCs reduces the group velocity of incident photons at that spectral region by the so-called "slow photon" effect. As a result, PL emission is enhanced due to increasing frequency of interactions between exciting photons and light-emitting molecules at that spectral region.<sup>25</sup> An alternative approach would be to tailor the intrinsic photoluminescence of NAA by engineering its structure in the form NAA-PCs. 53-54 Under this configuration, alignment of the NAA-PC's PSB with the Gaussian-like PL emission of NAA would narrow its linewidth by internally forbidding light propagation at specific spectral regions. Surprisingly, to the best of our knowledge, this system has not been explored yet.

This chapter shows how the intrinsic photoluminescence of NAA can be tuned by engineering its structure in the form of multispectral PCs (MS-NAA-PCs) — NAA-PCs featuring multiple PSBs at specific spectral positions (Figure 7.1).



**Figure. 7.1** Conceptual illustration showing the mechanism by which MS–NAA–PCs narrow PL emission from NAA by judicious alignment of PSBs. (a) Schematic showing the PL emission of a reference NAA (left) and a MS–NAA–PC (right). (b) Normalized reflection and PL spectra of a NAA film (top) and a MS–NAA–PC (bottom) showing the mechanism by which PSBs in MS–NAA–PCs are harnessed to selectively filter PL emission from NAA, where  $\lambda_{PL}$  and  $FWHM_{PL}$  represent the central wavelength position and full width at half maximum of the PL emission of NAA and MS–NAA–PCs, respectively.

Spectral alignment between the three characteristic PSBs of MS–NAA–PCs with the photoluminescence emission of NAA (Figure 7.1a) makes it possible to judiciously narrow its linewidth with precision by inhibiting light propagation at specific spectral positions (Figure 7.1b). These results create exciting new opportunities to modulate light emission from NAA-based structures, which could have broad implications across optoelectronic disciplines such as lasing, sensing, energy harvesting, and photocatalysis.

## 7.2 Experimental Details

#### 7.2.1 Fabrication of Reference NAA films

A set of NAA films featuring straight cylindrical nanopores from top to bottom were used as a reference material to quantify bulk PL emission. Al disc were anodized by the two-step process, full details of which are reported elsewhere. Briefly, before anodization Al chips were electropolished in a mixture of EtOH and  $HClO_4$  4:1 (v:v) at 20 V and 5 °C for 3 min. Then, the first anodization step was carried out in 0.3 M  $H_2C_2O_4$  aqueous electrolyte at 40 V and 5 °C for 20 h. Next, the resulting NAA layer was selectively removed by wet chemical etching in a mixture of 0.2 M  $H_2CrO_4$  and 0.4 M  $H_3PO_4$  for 3 h at 70 °C. After this, the second anodization step was performed under the same anodization conditions for a total charge density (integrated current density throughout time per unit of area) of 113.2 C cm<sup>-2</sup> under voltage control conditions at 40 V to generate a NAA film of 50  $\mu$ m featuring straight cylindrical nanopores.

#### 7.2.2 Fabrication of MS-NAA-PCs

Fabrication of MS–NAA–PCs was performed following a modified two-step anodization process. Electropolished Al discs were first anodized in a 0.3 M sulfuric acid electrolyte at 5°C under constant voltage at 25 V for 20 h. The NAA film was then chemically dissolved in a mixture of 0.2 M  $H_2$ CrO<sub>4</sub> and 0.4 M  $H_3$ PO<sub>4</sub> for 3 h at 70 °C. Then, a 10-min second step in the same acid electrolyte at 25 V for 10 min was applied to generate a shuttle layer for homogenous nanopore growth. Then, the anodization process was switched to sinusoidal pulse anodization under current density control conditions.

During this process, a sinusoidal current density input profile was applied to modulate nanopore diameter in depth and generate gradient-index filter PC structures.<sup>59</sup> MS–NAA–PCs consisted of a NAA layer featuring three gradient-index filters generated by judiciously modulating the anodizing current density waveform input into sequential sinusoids with three different pulse periods (i.e.,  $T_1$ ,  $T_2$  and  $T_3$ ), as described by Equation 7.1:

$$J(t) = \begin{cases} J_{1} \sin\left(\frac{2\pi}{T_{1}}t\right) + J_{0} & 0 \le t < NT_{1} \\ J_{1} \sin\left(\frac{2\pi}{T_{2}}t\right) + J_{0} & NT_{1} \le t < NT_{1} + NT_{2} \\ J_{1} \sin\left(\frac{2\pi}{T_{3}}t\right) + J_{0} & NT_{1} + NT_{2} \le t < NT_{1} + NT_{2} + NT_{3} \end{cases}$$
(7.1)

where J(t) is the anodization current density at time t (in seconds),  $J_1$  is the current density amplitude (in mA cm<sup>-2</sup>),  $T_i$  (i = 1, 2, 3) is the anodization period i (in seconds) and  $J_0$  is the offset current density (in mA cm<sup>-2</sup>). The offset current density ( $J_0$ ), current density amplitude ( $J_1$ ) and number de periods (N) were kept constant

throughout the anodization process for all MS–NAA–PCs fabricated in this study, while the anodization periods were varied as  $T_1$  = 125 s,  $T_2$  = 150 s, and  $T_3$  = 175 s for N = 100 pulses per period ( $N_1$ ,  $N_2$  and  $N_3$ ) (i.e., total of 300 pulses). After this, a 50  $\mu$ m thick NAA layer produced in 0.3 M oxalic electrolyte (i.e., light-emitting layer) was generated under potentionstatic conditions at 40 V. **Table 7.1** summarizes the fabrication conditions used to fabricate MS–NAA–PCs. After anodization, the remaining aluminum substrate was removed from the backside of MS–NAA–PCs by selective chemical etching in a saturated solution of HCl and CuCl<sub>2</sub> for optical characterization.

**Table 7.1.** Fabrication conditions of MS–NAA–PCs including current density amplitude  $(J_1)$ , anodization period  $(T_i)$  and offset current density  $(J_0)$ .

	$J_0$ (mA cm <sup>-2</sup> )		-	-	3	N <sub>1</sub> (pulses)	N <sub>2</sub> (pulses)	N <sub>3</sub> (pulses)
MS-NAA-PCs	1.98	1.41	125	150	175	100	100	100

## 7.2.3 Optical Characterization of MS-NAA-PCs

Reflection spectra from MS–NAA–PCs were measured from 250 to 900 nm with a resolution of 2 nm at varying angle of incidence, from 8 to 65°, in a PerkinElmer UV–visible–NIR Lambda 950 spectrophotometer. Reflection intensity ( $R_{PSB}$ ), position of central wavelength ( $\lambda_{PSB}$ ), and full width at half-maximum ( $FWHM_{PSB}$ ) of the photonic stopbands (PSBs) of MS–NAA–PCs were estimated from reflection spectra through Gaussian fittings performed in OriginPro8.5®. PL spectra from MS–NAA–PCs were acquired in a fluorescence spectrophotometer (Photon Technology International Inc., Division of Horiba, USA) equipped with a Xe lamp as excitation light

source at room temperature and at an excitation wavelength ( $\lambda_{ex}$ ) of 355 nm. PL measurements were performed from the top side of reference NAA films and MS–NAA–PCs, using a commercial bandpass filter with a cutoff wavelength of 350 nm.

#### 7.2.4 Structural Characterization of MS-NAA-PCs

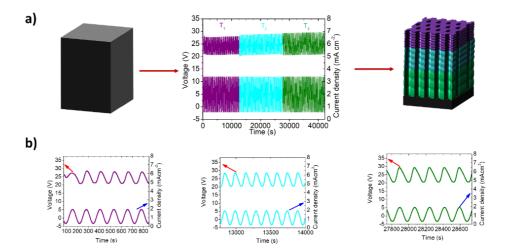
Morphological and structural features of NAA films and MS–NAA–PCs were characterized by a field-emission gun scanning electron microscope (FEG-SEM FEI Quanta 450) operating at an accelerating voltage of 20–25 keV. Characteristic geometric features of MS–NAA–PCs were quantified by analyzing FEG-SEM images in ImageJ software.<sup>60</sup>

#### 7.3. Results and Discussion

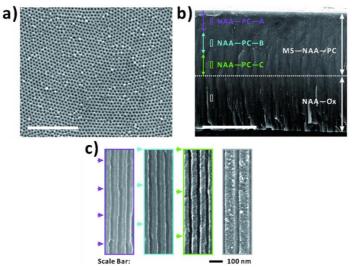
#### 7.3.1Fabrication and Structural Characterization of MS-NAA-PCs

**Figure 7.2a** illustrates the fabrication process used to produce the light-filtering layer of MS–NAA–PCs under sinusoidal current density conditions, including a full-view of a representative anodization profile. **Figure 7.2b** shows magnified views of this sinusoidal pulse anodization process, in which the current density period (Ti) — time between consecutive sinusoidal pulses — is increased from 125 to 175 s with a step size of  $\Delta Ti = 25$  s after each 100 pulses. This input current density profile results in three stacked layers of NAA featuring a modulated nanopore diameter in depth, each of which represents a gradient-index filter with its characteristic PSB. As such, the optical response of the composite NAA–PC features three PSBs, one for each NAA gradient-index filter composing the overall PC structure. It is apparent from these graphs that, under the

fabrication conditions used in this study, the sinusoidal current density input with  $J_0 = 1.98$  mA cm<sup>-2</sup>,  $J_1 = 1.41$  mA cm<sup>-2</sup>,  $T_1 = 125$  s,  $T_2 = 150$  s, and  $T_3 = 175$  s for a total of 300 pulses is precisely translated into a sinusoidal voltage output, which mimics the frequency of the input profile. Analysis of this anodization profile indicates that the amplitude of the sinusoidal voltage output slightly increases with increasing  $T_i$ , from ~20–25 V at T1 = 125 s to ~20–29 V at  $T_3$ , respectively. **Figure 7.3a** shows a top view FEG-SEM image of this NAA–PC structure, which features hexagonally arranged, homogeneously distributed nanopores across its surface. The average nanopore diameter estimated from FEG-SEM image analysis was  $17 \pm 4$  nm, while the interpore distance — distance between center of adjacent nanopores — was measured to be  $62 \pm 5$  nm.



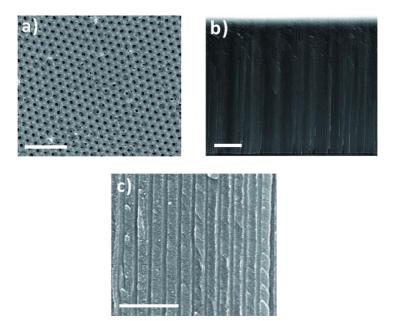
**Figure. 7.2** Fabrication of MS–NAA–PCs by sinusoidal pulse anodization. (a) Schematics of fabrication process to produce MS–NAA–PCs by a sinusoidal current density profile with three anodization periods ( $T_1$ ,  $T_2$  and  $T_3$ ) including aluminum substrate (left), representative full-view anodization profile with current density input and voltage output (center) and resulting MS–NAA–PC featuring three stacked gradient-index filters (right). (b) Magnified views of sinusoidal current density profile shown in (a) for each anodization period ( $T_1$ ,  $T_2$  and  $T_3$ ) demonstrating the precise translation of current density pulses into sinusoidal voltage output pulses.



**Figure. 7.3.** Structural characterization of MS–NAA–PCs. (a) Top view FEG-SEM image of a representative MS–NAA–PC featuring average nanopore diameter and interpore distance of 17 ± 4 nm and 62 ± 5 nm, respectively (scale bar = 1 μm). (b) Full-view cross-sectional FEG-SEM image of a MS–NAA–PC featuring a light-filtering layer at its top and a light-emitting layer at its bottom with thicknesses of 58 ± 1 mm and 50 ± 1 μm, respectively, and NAA–PC–A, NAA–PC–B and NAA–PC–C denote NAA gradient-index filters produced with  $T_1$  = 125 s,  $T_2$  = 150 s, and  $T_3$  = 175 s, respectively, and NAA–Ox corresponds to the light-emitting layer at the bottom of the NAA–PC structures (scale bar = 50 μm). (c) Magnified view cross-sectional FEG-SEM images of color rectangles shown in (b) showing details of nanopore diameter modulations in NAA–PC–A, NAA–PC–B and NAA–PC–C, and straight cylindrical nanopores in NAA–Ox layer (NB: color arrows denote nanopore modulations).

**Figure 7.3b** shows a general cross-sectional view FEG-SEM image of these NAA–PCs, from which is it possible to discern two main layers: i) a top light-filtering layer formed by three NAA gradient index filters labelled as NAA–PC–A ( $T_1$  = 125 s), NAA–PC–B ( $T_2$  = 150 s) and NAA–PC–C ( $T_3$  = 175 s), which feature modulated nanopore diameter in depth; and ii) a bottom light-emitting layer featuring straight cylindrical nanopores at the bottom labelled as NAA–Ox. The thicknesses of the top and bottom layers were 58 ± 1 and 50 ± 1 μm, respectively, according to FEG-SEM image analysis. **Figure 7.3c** shows a set of magnified cross-sectional views showing details of nanopores at specific positions of the top and bottom layers of the MS–NAA–PC structure. FEG-SEM images of the NAA gradient-index filters

forming the top light-filtering layer reveal nanopore modulations, the period length ( $L_{TP}$ ) of which increases with the input anodization period ( $T_i$ ). Analysis of this geometric parameter for NAA–PC–A, NAA–PC–B and NAA–PC–C reveals that  $L_{TP}$  increases linearly with  $T_i$  at a rate of 2.1  $\pm$  0.1 nm s<sup>-1</sup>, having values of 210  $\pm$  4, 265  $\pm$  6, and 313  $\pm$  8 nm for  $T_1$ ,  $T_2$  and  $T_3$ , respectively. Figure 7.3c also shows a magnified cross-sectional view of the light-emitting layer at the bottom of the MS–NAA–PC structure, which was fabricated in 0.3 M oxalic acid electrolyte at 40 V for a total of ~16 h. This layer features straight cylindrical nanopores with constant diameter from top to bottom. A set of FEG-SEM images of this film from a control NAA–Ox sample used to characterize the bulk PL emission of this layer is shown in Figure 7.4. The 50 mm-thick layer features straight cylindrical nanopores with an average diameter of 40  $\pm$  3 nm and an interpore distance of 101  $\pm$  6 nm.



**Fig 7.4.** Structural characterization of NAA. (a) Top view FEG-SEM image of a representative NAA (scale bar = 500 nm). (b) Full-view cross-sectional FEG-SEM image of a NAA with thicknesses  $50 \pm 1$  mm, (scale bar = 100 mm). (c) Magnified view cross-sectional FEG-SEM showing details of the nanopore s (scale bar = 100 nm).

## 7.3.2 Optical Characterization of MS-NAA-PCs.

MS-NAA-PCs can be optically described as heterogeneous PC structures with a spectroscopic signature that results from the multiple contributions of the NAA-based gradient-index filters composing their structure (i.e., NAA-PC-A, NAA-PC-B and NAA-PC-C). As such, the reflection spectrum of MS-NAA-PCs features three well-resolved, intense PSBs, the features of which are critically determined by the structural features of each NAA gradient-index filter engineered by the input current density profile.

The light-filtering layer on the top side of MS–NAA–PCs filters the photon-stimulated PL emission from the light-emitting layer at the bottom side of the MS–NAA–PC structure. Therefore, it is critical to characterize and understand the angle-dependence of both light reflection and light emission at the light-filtering and light-emitting layers of the MS–NAA–PC structure, respectively.

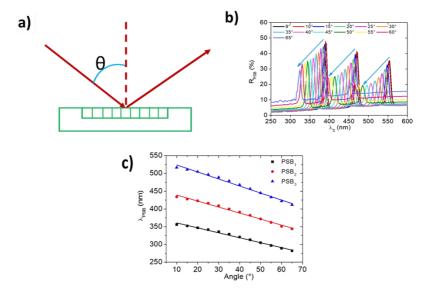
### 7.3.3 Effect of the Incidence Angle in the PSBs of MS-NAA-PCs

The effect of the incidence angle ( $\theta$ ) on the optical features of the PSBs of MS–NAA–PCs was systematically evaluated by reflection spectroscopy (**Figure 7.5a**). **Figure 7.5b** shows the reflection spectra of MS–NAA–PCs at different incidence angles (i.e.,  $8^{\circ}$ ,  $10^{\circ}$ ,  $15^{\circ}$  20°,  $25^{\circ}$ ,  $30^{\circ}$ ,  $35^{\circ}$ ,  $40^{\circ}$ ,  $45^{\circ}$ ,  $50^{\circ}$ ,  $55^{\circ}$ ,  $60^{\circ}$  and  $65^{\circ}$ ). **Table 7.2** summarizes the optical features of the three characteristic PSBs of NAA–PC–A, NAA–PC–B, and NAA–PC–C labelled as PSB<sub>1</sub>, PSB<sub>2</sub>, and PSB<sub>3</sub>, including the central wavelength position ( $\lambda_{PSB}$ ), reflection intensity ( $R_{PSB}$ ), and full width at half maximum ( $FWHM_{PSB}$ ), all estimated from Gaussian fittings.

The position of the three PSBs in the reflection spectrum of MS–NAA–PCs blue-shifts, while their intensity decreases with increasing angle of incidence. This result is in good agreement with the Bragg–Snell law, in which the wavelength of the diffracted light depends on the angle of incidence, the periodicity, and the effective refractive index<sup>61-63</sup> of the nanoporous PC as expressed in Equation 7.2:

$$m\lambda_{PSB} = 2L_{TP} \sqrt{n_{eff}^2 - \sin^2\theta}$$
 (7.2)

where  $\lambda_{PSB}$  is the central wavelength of the PSB, m is the order of the PSB,  $L_{TP}$  is the structure periodicity,  $\theta$  is the angle of incidence, and  $n_{eff}$  is the effective refractive index. Analysis of this dependence, summarized in **Figure 7.5c**, shows that  $\lambda_{PSB}$  is blue shifted at rates of  $-1.22 \pm 0.04$ ,  $-1.49 \pm 0.05$ , and  $-1.78 \pm 0.06$  nm deg<sup>-1</sup> for PSB<sub>1</sub>, PSB<sub>2</sub> and PSB<sub>3</sub>, respectively.



**Figure. 7.5.** Effect of the incidence angle on the optical features of the PSBs of MS–NAA–PCs. (a) Schematic showing the variation of the incidence angle. (b) Reflection spectra of a representative MS–NAA–PC as a function of angle of incidence, from  $\theta$  = 8° to 65°. (c) Central wavelength position of MS–NAA–PC's PSB<sub>1</sub>, PSB<sub>2</sub> and PSB<sub>3</sub> ( $\lambda_{PSB}$ ) as a function of  $\theta$ .

Table 7.2. Summary of optical features of MS-NAA-PCs.

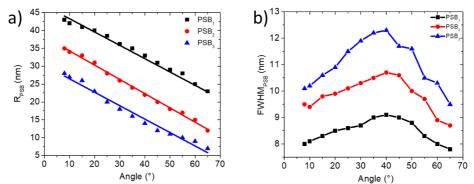
Angle		3 P FINITING		
(°)	Band	λ <sub>band</sub> (nm)	R <sub>band</sub> (%)	FWHM (nm)
	1	390	43.0	8.0
8	2	470	35.0	9.5
	3	553	28.0	10
	1	389	42.6	8.1
10	2	469	35.0	9.4
	3	551	28.0	10.2
	1	387	42.0	8.3
15	2	466	33.0	9.8
	3	548	26.0	10.6
	1	382	40.0	8.5
20	2	461	31.0	9.9
	3	541	23.0	11.0
	1	377	38.5	8.6
25	2	455	28.5	10.1
	3	534	20.7	11.5
	1	372	36.2	8.7
30	2	448	26.2	10.3
	3	526	18.2	12.0
	1	365	35.0	9.0
35	2	440	24.1	10.5
	3	516	16.0	12.2
	1	358	33.0	9.1
40	2	431	22.0	10.7
	3	506	14.0	12.3
	1	351	31.4	9.0
45	2	422	20.0	10.6
	3	495	12.4	11.7
	1	344	29.6	8.8
50	2	413	18.2	10.0
	3	485	11.6	10.6
	1	336	28.0	8.3
55	2	404	17.0	9.7
	3	474	10.5	10.5
	1	329	25.0	8.0
60	2	396	15.0	8.9
	3	464	9.0	10.3
	1	323	19.0	7.8
65	2	388	12.5	8.9
	3	455	7.0	9.5

**Figure 7.6** shows the dependence of  $R_{PSB}$  and  $FWHM_{PSB}$  as a function of incidence angle, which indicates that the reflection intensity of the PSB decreases with increasing angle of incidence. Analysis of the fitting lines shown in **Figure 7.6a** denotes that  $R_{PSB}$  decreases at rates of  $-0.37 \pm 0.02$ ,  $-0.39 \pm 0.007$ ,  $-0.38 \pm 0.016$  a.u.  $deg^{-1}$  for PSB<sub>1</sub>, PSB<sub>2</sub>, and PSB<sub>3</sub>, respectively.

It is apparent from **Figure 7.6b** that the dependence of  $FWHM_{PSB}$  with angle of incidence follows a Gaussian-like trend, where this optical feature increases until 40° and dramatically decreases > 45° until 65°. Trends for  $FWHM_{PSB}$ 's PSB<sub>1</sub>, PSB<sub>2</sub>, and PSB<sub>3</sub>, were determined to be:

- a)  $FWHM_1 = 7.53 + ((64.63)/(34.64 \cdot p/2) \cdot Exp(-2 \cdot (\theta 36.59/(34.65)))$
- b)  $FWHM_2 = -4.74 + ((2363.2)/(123.63 \cdot p/2) \cdot Exp(-2 \cdot (\theta 33.84/(123.63)))$
- c)  $FWHM_3 = 9.19 + ((125.62)/(33.0 \cdot p/2) \cdot Exp(-2 \cdot (\theta 35.92/(33.0)))$

from Gaussian fittings, respectively.



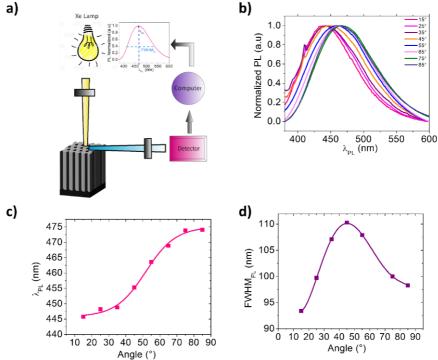
**Figure 7.6.** Effect of the angle of incidence on the PSB's features of MS–NAA–PCs. (a) Reflection intensity of PSB ( $R_{PSB}$ ) as functions of  $\vartheta$ . (b) Full width at half-maximum of PSB ( $FWHM_{PSB}$ ) as functions of  $\vartheta$ .

# 7.3.4 Effect of the Incidence Angle in the PL of the Light-Emitting Layer in MS-NAA-PCs

Photoluminescence of NAA is attributable to oxygen vacancies distributed across the onion-like composition of anodic alumina, and oxalic impurities incorporated into its structure from the acid electrolyte during the anodization process. Of all types, NAA produced in oxalic acid electrolyte has the highest PL emission.<sup>49-51</sup> Conversely, the characteristic PL emission from NAA produced in sulfuric acid electrolyte is weak and almost negligible by comparison. For this reason, we devised the structure of MS–NAA–PCs featuring a top light-filtering layer having an almost negligible PL emission and a bottom light-emitting layer with strong PL emission. **Figure 7.7a** shows a schematic illustration of the experimental setup used to characterize PL emissions from MS–NAA–PCs.

**Figure 7.7b** shows the characteristic PL emission at different angles of incidence (from 15° to 85° with an interval of 10°) from a representative 50 μm-thick NAA film fabricated by two-step anodization in oxalic acid electrolyte. The emission spectrum of the NAA film is characterized by a broad, intense Gaussian-like emission band across the 380–600 nm range for all the angles of incidence analyzed. It is apparent from **Figure 7.7c** that the position of the PL band ( $\lambda_{PL}$ ) is shifted toward longer wavelengths (i.e., red shift) with increasing angle of incidence, following a sigmoidal trend where  $\lambda_{PL}$  = 475.04 + (445.8—475.04)/1 + Exp (θ–51.67/ 8.82). This graph indicates a slight red shift of  $\lambda_{PL}$  with θ, from 445 nm at 15° to 448 nm at 35°. However,  $\lambda_{PL}$  undergoes a significant shift between 35° and 75°, in which  $\lambda_{PL}$  red-shifts its position from 448 nm to 479 nm, respectively, and it stabilizes its position for θ > 75°.

**Figure 7.7d** shows the dependence of  $FWHM_{PL}$  with the angle of incidence. It is apparent that  $FWHM_{PL}$  follows a Gaussian-like trend with  $\theta$ , where this optical feature initially increases with angle of incidence until  $45^{\circ}$ . At this angle,  $FWHM_{PL}$  achieves its maximum value of  $115 \pm 1$  nm. For  $\theta > 45^{\circ}$ ,  $FWHM_{PL}$  starts to decrease until a minimum of  $98 \pm 2$  nm at an angle of  $85^{\circ}$ . **Table 7.3** summarizes the dependence of  $\lambda_{PL}$  and  $FWHM_{PL}$  with the angle of incidence for a representative light-emitting NAA film produced in oxalic acid electrolyte.



**Figure 7.7.** Photoluminescent emission from NAA films. (a) Schematic illustration of the PL setup used to characterize PL emission from MS–NAA–PCs and NAA–Ox films. (b) Characteristic Gaussian-like PL emission at varying the angle of incidence, from 15° to 85°, from a reference NAA–Ox film fabricated in oxalic acid electrolyte by two step anodization (NB:  $\lambda_{ex}$  = 350 nm). (c) Dependence of central wavelength position of PL emission ( $\lambda_{PL}$ ) with angle of incidence. (d) Dependence of full width at half maximum of PL emission ( $FWHM_{PL}$ ) with angle of incidence.

**Table 7.3**. Photoluminescence wavelength of NAA–Ox light-emitting layer produced in oxalic acid at different angles.

Angle (°)	PL wavelength (nm)	FWHM (nm)
15	445	93
25	448	100
35	448	107
45	455	110
55	464	108
65	469	105
75	474	100
85	474	98

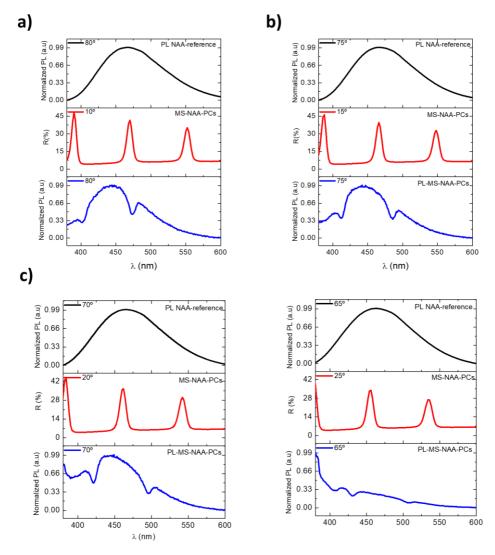
#### 7.3.5 Photoluminescence of MS-NAA-PCs.

MS–NAA–PCs were fabricated to feature three well-resolved PSBs as specific spectral positions within the PL emission of NAA–Ox films. To this end, the structure of MS–NAA–PCs was judiciously engineered with three stacked gradient-index filters embedded within the same heterogeneous PC structure. These heterogeneous NAA-based PCs were used as model platforms to study for the first time the light-filtering properties of NAA–PCs, harnessing the intrinsic light-emitting properties of NAA. MS–NAA–PCs were mounted on a rotating stage, which allows PL signal to be measured at different angles. Excitation light at 355 nm was shone onto the center of MS–NAA–PCs and the emission was collected from 380 to 600 nm at varying angle of incidence. Figure 7.8 shows the PL emission of a reference NAA–Ox film (black line), and the reflection (red line) spectrum, and PL emission (blue line) of a MS–NAA–PCs at varying angle of incidence (i.e., 65°, 70°, 75°, and 80° for PL, and

complementary reflection angles of 25°, 20°, 15°, and 10° for reflection, respectively). It is apparent that the generation of three gradient-index filters on top of the light-emitting NAA–Ox layer filters efficiently PL emission by narrowing  $FWHM_{PL}$  and shifting  $\lambda_{PL}$  following an angle-dependent pattern.  $FWHM_{PL}$  of the PL emission of the NAA–Ox film at 80°, 75°, 70°, and 65° was measured to be 99  $\pm$  2, 100  $\pm$  2, 103  $\pm$  1, and 105  $\pm$  1 nm, respectively (Figures 7.8a–d). Upon the generation of a MS–NAA–PCs,  $FWHM_{PL}$  is narrowed to 93  $\pm$  2, 88  $\pm$  2, 97  $\pm$  3, and 88  $\pm$  6 nm at 80°, 75°, 70°, and 65°, respectively. This result indicates that light emission is filtered by the top gradient-index filters. It is also found that  $\lambda_{PL}$  red-shifts its position with decreasing angle of incidence, having values of 443  $\pm$  1, 447  $\pm$  1, 451  $\pm$  1, and 450  $\pm$  1 nm at 80°, 75°, 70°, and 65°, respectively (Figures 7.8a–d).

For instance, the PL emission of MS–NAA–PCs at 80° (**Figure 7.8a**) shows two local minima or shoulders at 402 and 473 nm, which would correspond to light-emitting inhibition associated with PSB<sub>1</sub> (389 nm) and PSB<sub>2</sub> (461 nm), respectively. At that angle of incidence, PSB<sub>3</sub> (551 nm) is far from the main Gaussian-like PL emission. Therefore, it is inferred that this gradient-index filter does not contribute to the filtered PL emission from the MS–NAA–PC structure within this spectral region. Upon reduction of the angle of incidence, the characteristic PBSs of the MS–NAA–PC structure undergo a blue shift, which in turn changes the characteristics of the light beam emitted from the underlying NAA film. **Figure 7.8b** shows that the local minima of the PL emission from MS–NAA–PCs at 75° features two local minima at 412 and 486 nm, which would correspond

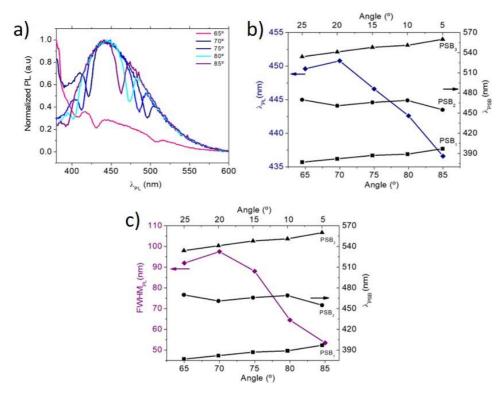
to light-emitting inhibition associated with  $PSB_1$  (387 nm) and  $PSB_2$  (466 nm), respectively. At that angle of incidence,  $PSB_3$  is located at 548 nm, which is still far from the spectral position of the PL emission and does not contribute significantly to filtering.



**Figure 7.8**. Photoluminescence emission of MS–NAA–PC with PL spectra of NAA of oxalic acid as a reference (black line), reflection spectra of MS–NAA–PC (red line), and PL spectra of MS–NAA–PC (blue line) at: (a) 10° (reflection) and 80° (PL emission), (b) 15° (reflection) and 75° (PL emission), (c) 20° (reflection) and 70° (PL emission), and (d) 25° (reflection) and 65° (PL emission) (NB: angles of reflection and emission were complementary at  $25^{\circ} - \theta_{reflection} + \theta_{emission} = 90$ °).

Figure 7.8c shows that the local minima of the PL emission of MS–NAA–PCs at 70° features two local minima at 421 and 497 nm, which would correspond to light-emitting inhibition associated with PSB<sub>1</sub> (382 nm) and PSB<sub>2</sub> (466 nm), respectively. At that angle of incidence, PSB<sub>3</sub> is located at 541 nm, which is still far from the spectral position of the PL emission and does not contribute significantly to filtering. Figure 7.8d shows that the local minima of the PL emission of MS–NAA–PCs at 65° features two local minima at 430 and 507 nm, which would correspond to light-emitting inhibition associated with PSB<sub>1</sub> (377 nm) and PSB<sub>2</sub> (455 nm), respectively. At that angle of incidence, PSB<sub>3</sub> is located at 541 nm, which is still far from the spectral position of the PL emission and does not contribute significantly to PL emission filtering.

To gain further insight into the light-filtering properties of MS–NAA–PCs and the dependence of PL emission, we analyzed the optical features of PL emission at distinct angle of incidence. At first glance, **Figure 7.9a** reveals an interesting effect where light emitted from the underlying photoluminescent layer is narrowed and shifted with the angle of incidence. **Figures 7.9b and c** summarize the positions of the characteristic PSB<sub>1</sub>, PSB<sub>2</sub>, and PSB<sub>3</sub>, and the features of the PL emission (*FWHM* $_{PL}$  and  $\lambda_{PL}$ ) from MS–NAA–PCs. It is apparent that the position of PL emission ( $\lambda_{PL}$ ) undergoes a slight red shift when the angle of incidence is increased from 65° to 70° (i.e., from 450 to 451 nm, respectively) (**Figure 7.9b**). After this point, the light-filtering layer of MS–NAA–PCs blue-shifts the position of the Gaussian-like PL emission from the light-emitting NAA–Ox layer at the bottom of the heterogenous NAA–PC structure. PL emission from 70° to 85° is found to blue shift linearly from 451 to 437 nm, at a rate of ~–0.93 nm deg<sup>-1</sup>.



**Figure 7.9.** Summary of the position of the PSB<sub>1</sub>, PSB<sub>2</sub> and PSB<sub>3</sub> and the features of PL emission from MS–NAA–PCs (NB: angles of reflection and emission were complementary at 25° –  $\theta$  reflection +  $\theta$  emission = 90°). (a) PL emission from MS–NAA–PCs at 65°, 70°, 75°, 80° and 85°. (b) Dependence of  $\lambda_{PL}$  and the position of the PSB<sub>1</sub>, PSB<sub>2</sub> and PSB<sub>3</sub> in MS–NAA–PCs with angle of incidence. (c) Dependence of FWHM<sub>PL</sub> and the position of the PSB<sub>1</sub>, PSB<sub>2</sub> and PSB<sub>3</sub> in MS–NAA–PCs with angle of incidence.

Dependence of *FWHM<sub>PL</sub>* with angle of incidence is found to follow a qualitatively similar trend. Initially, PL emission is slightly widened, from 65° to 70°, where this optical feature increases from 92 to 97 nm, respectively (**Figure 7.9c**). However, the light-filtering layer of MS–NAA–PCs can efficiently narrow PL emission from 70° to 85°, where *FWHM<sub>PL</sub>* is found to be sharply and linearly narrowed from 97 to 54 nm, at a rate of ~3.11 nm deg<sup>-1</sup>. These results clearly demonstrate that a smart structural design of NAA–PCs can be judiciously harnessed to tune and control the features of the intrinsic photoluminescence emission of this highly tailorable platform material.

#### 7.4 Conclusion

In this Chapter, we demonstrated the structural tuning of intrinsic photoluminescence emissions from nanoporous anodic alumina photonic crystals. We have harnessed a smart structural design in which a non-emitting, light-filtering layer in the form of multispectral NAA-PC is combined with an intrinsically light-emitting layer of NAA. MS-NAA-PCs feature three intense, well-resolved photonic stopbands, the positions of which can be spaced across the visible spectrum from ~380 to 560 nm. Judicious -emitting NAA layer. This approach makes it possible to engineering of three photonic stopbands in the top light-filtering layer has been demonstrated as an effective approach to narrow and tune photoluminescence emission from an underlying light narrow the width of photoluminescence emission up to ~50 nm, and blue-shift its position for ~15 nm. Inhibition of light emission is accomplished by harnessing forbidden light propagation through the characteristic photonic stopbands of the top light-filtering layer. MS-NAA-PCs enable control over intrinsic photoluminescence of NAA, without the use of external PL emitters such as dyes and fluorophores. These findings provide exciting new opportunities to engineer the intrinsic light-emitting properties of NAA-based photonic crystals structures, which have implications across a variety of photonic technologies such as sensing and biosensing, lasing and light sources, photodetection, photocatalysis, green energy generation and solar light harvesting.

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# Chapter 8. Summary and Conclusion

UNIVERSITAT ROVIRA I VIRGILI ENGINEERING OF PHOTONIC STRUCTURES BASED ON NANOPOROUS ANODIC ALUMINA AS AN OPTICAL SENSING PLATFORM Laura Karen Acosta Capilla During the development of this thesis, the engineering of Photonic structures based on Nanoporous Anodic Alumina was explored. Furthermore, different photonic structures were fabricated and used as optical sensor with different analytes such as: D-Glucose, alcohols mixtures and sodium chloride.

In **chapter 2** we presented the state of the art of NAA. In this chapter we presented a summary of the historical background of NAA. The NAA structure, fabrication, anodization techniques as well as the anodization parameters and geometrical characteristics.

In **Chapter 3** we presented the fundamentals of Photonic Structures Based on Nanoporous anodic alumina. The background of this structures was explored. In addition, the different anodization approaches to obtain the most important photonic structures such as: Fabry Pérot interferometers (FPI), Gradient index Filters (GIFs), Distributed Bragg Reflectors (DBRs), microcavities ( $\mu$ CVs), multispectral photonic structures and Bandpass filters (BPFs). Moreover, the potential applications of these structures were presented like optical sensors, Photocatalysis, Drug Delivery and Optical encoding.

In **Chapter 4** we presented the development and optical engineering of stacked nanoporous anodic alumina photonic structures with multispectral bands. (NAA-MPSs) with tunable multi-spectral photonic stopbands for sensing applications. The structure of these photonic crystal (PC) is formed by stacked layers of NAA produced with sinusoidally modified effective medium. The progressive modification of the sinusoidal period during the anodization process enables the generation and precise tuning of the characteristic photonic stopbands. The position of the

forbidden bands presented by these multi-spectral NAA-MPSs can be accurately tuned by varying the anodization period of the anodization current density waveform. Furthermore, we assess the effect of the porosity of the structure on the reflection spectrum by applying a pore widening chemical etching treatment from 0 to 25 min. We also demonstrated the ability of multi-spectral NAA-MPSs structures for sensing applications by detecting small changes of the effective refractive index due to the fluid filling of the pores. Different concentrations of D-glucose have been successfully detected and quantified in real-time. These real-time experiments, carried out by increasing the average pore diameter from 35 nm to 55 nm, indicate that the sensitivity is different for each forbidden band and also it depends on the pore diameter of the multi-spectral NAA-MPS structure: the increment of the pore diameter leads to an enhancement in sensitivity of the photonic crystal structure.

In **Chapter 5** we present a Gaussian pulse anodization approach to generate nanoporous photonic crystals with highly tunable and controllable optical properties across the visible—NIR spectrum. Nanoporous anodic alumina Gaussian photonic crystals (NAA-GPSs) are fabricated in oxalic acid electrolyte by Gaussian pulse anodization a novel form of pulse-like anodization. We evaluate the effect of the Gaussian pulse width in the anodization profile on the optical properties of these photonic crystals by systematically varying this fabrication parameter from 5 to 60 s. The optical features of the characteristic photonic stopband (PSB) of NAA-GPSs position of central wavelength, full width at half maximum and intensity are found to be highly dependent on the Gaussian pulse width, the incidence angle of incoming photons and the nanopore diameter of NAA-GPSs. The effective medium of NAA-GPSs was

assessed by monitoring spectral shifts in their characteristic PSB upon infiltration of their nanoporous structure with analytical solutions of D-glucose of varying concentration (0.0125–1 M). The findings demonstrate that Gaussian pulse anodization is an effective nanofabrication approach to produce highly sensitive NAA-based PC structures with versatile and tunable PSBs across the spectral regions.

In Chapter 6 Nanoporous anodic alumina optical microcavities (NAAμQVs) with spectrally tunable resonance band and surface chemistry were used as model light-confining photonic crystal (PC) platforms to elucidate the combined effect of spectral light confinement features and surface chemistry on optical sensitivity nm-1 in water- and organic-based analytical solutions, respectively. The nanoporous architecture of NAAμQVs featuring two distributed Bragg mirrors with a physical cavity layer in between was engineered by stepwise pulse anodization. Model NAAμQVs showed well-resolved, spectrally tunable resonance bands ~400 to 800 nm by careful modification of the anodization period in the input STPA profile NAA-µQVs was assessed by analyzing dynamic spectral shifts of NAA-μQVs' resonance band upon infiltration with organic- and aqueousbased analytical solutions of equally varying refractive index, from 1.333 to 1.345 RIU. The findings demonstrated that optical sensitivity of both hydrophilic and hydrophobic NAA-μQVs increases linearly with the position of their characteristic resonance, in both organic and aqueous solutions, due to increasing optical absorbance. Analysis of sensitivity also revealed that hydrophilic NAA-μQVs show ~81 and 35 % superior sensitivity to their hydrophobic counterparts for organic- and aqueousbased analytical solutions, respectively. This chapter provides a new avenue to explore the unique light-confining properties of NAA-based PC structures for optical sensing applications. Precise design and engineering of structural, optical, and chemical properties of these PCs provide exciting new opportunities to harness distinct forms of light–matter interactions for a broad range of photonic technologies and sensing applications.

In Chapter 7 We demonstrated the precise structural engineering and tuning of intrinsic photoluminescence emissions from nanoporous anodic alumina photonic crystals (NAA-PCs). A smart structural design by a combination of pulse and constant anodization in distinct acid electrolytes makes it possible to engineer a novel heterogenous optical structure consisting of a non-emitting, light-filtering layer in the form of multispectral NAA-PC, and an intrinsically light-emitting layer of NAA. MS-NAA-PCs are engineered to feature three intense, well-resolved photonic stopbands, the position of which are spaced across the visible spectrum, from ~380 to 560 nm. This approach makes it possible to engineering of three photonic stopbands in the top light-filtering layer has been demonstrated effective approach to narrow and tune as an photoluminescence emission from an underlying light narrow the width of photoluminescence emission up to ~50 nm, and blue-shift its position for ~15 nm. Inhibition of light emission is accomplished by harnessing forbidden light propagation through the characteristic photonic stopbands of the top light-filtering layer.

In summary, all the data and work presented in this thesis demonstrated the ability of the Photonic structures based on Nanoporous Anodic Alumina as a potential platform for develop optical sensors.